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ERDMAN ANTHONY ASSOCIATES ROCHESTER NY
NATIONAL DAM SAFETY PROGRAM, DAVIS BROOK DAM (SITE 1) (INVENTOR--ETC(U)
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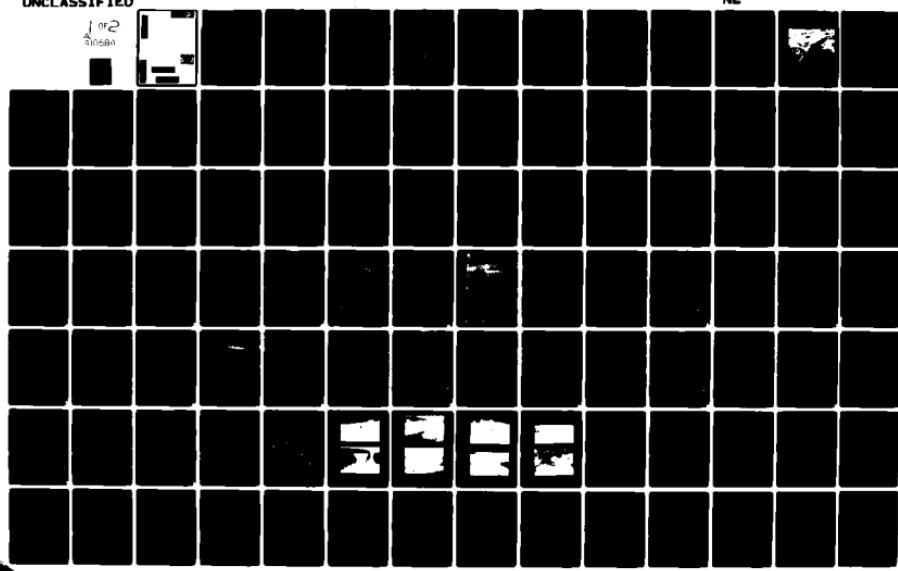
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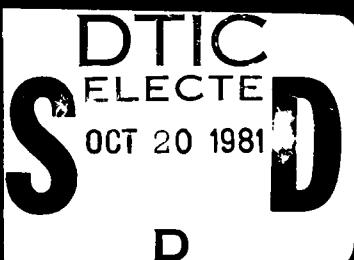
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20. ABSTRACT (Continue on reverse side if necessary and identify by block number) This report provides information and analysis on the physical condition of the dam as of the report date. Information and analysis are based on visual inspection of the dam by the performing organization. Examination of available documents and visual inspection of Conewango Creek Watershed Davis Brook Dam (Site 1) and appurtenant structures did not reveal conditions which constitute a hazard to human life or property. However, the dam has some deficiencies which require further investigation and remedial action.		

A wet condition of unknown cause was observed on the lower portion of the left downstream slope. It is recommended that the services of a qualified registered professional engineer be retained to evaluate this condition.

Using the Corps of Engineers screening criteria for review of spillway adequacy, it has been determined that the dam would not be overtopped under full PMF conditions. The PMF routed through the reservoir required only 46 percent of the spillway outflow capacity. The spillway capacity is therefore judged as adequate.

The recommended investigation should be completed within 12 months of notification to owner, and remedial actions resulting from these investigations completed in the subsequent 12 months.

The following remedial measures should be performed within 1 year of notification to owner:

- Develop a formal downstream warning system.
- Develop and maintain a program of periodic technical inspections.
- Implement a program of diligent and periodic maintenance.
- Remove trees and brush from slopes.
- Regrade and fill in the erosion gullies.
- Install ladder rungs on the riser.

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ALLEGHENY RIVER BASIN

**CONEWANGO CREEK WATERSHED
DAVIS BROOK DAM (SITE 1)**

**CATTARAUGUS COUNTY, NEW YORK
INVENTORY No. N.Y. 564**

**PHASE I INSPECTION REPORT
NATIONAL DAM SAFETY PROGRAM**



NEW YORK DISTRICT, CORPS OF ENGINEERS

AUGUST 1981

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PREFACE

This report is prepared under guidance contained in the Recommended Guidelines for Safety Inspection of Dams for Phase I Investigations. Copies of these guidelines may be obtained from the Office of Chief of Engineers, Washington, D.C. 20314. The purpose of a Phase I Investigation is to identify expeditiously those dams which may pose hazards to human life or property. The assessment of the general condition of the dam is based upon available data and visual inspections. Detailed investigation and analyses involving topographic mapping, subsurface investigations, testing, and detailed computational evaluations are beyond the scope of a Phase I Investigation; however, the Investigation is intended to identify any need for such studies.

In reviewing this report, it should be realized that the reported condition of the dam is based on observations of field conditions at the time of inspection along with data available to the inspection team. In cases where the reservoir was lowered or drained prior to inspection, such action, while improving the stability and safety of the dam, removes the normal load on the structure and may obscure certain conditions which might otherwise be detectable if inspected under the normal operating environment of the structure.

It is important to note that the condition of a dam depends on numerous and constantly changing internal and external conditions, and is evolutionary in nature. It would be incorrect to assume that the present condition of the dam will continue to represent the condition of the dam at some point in the future. Only through frequent inspections can unsafe conditions be detected and only through continued care and maintenance can these conditions be prevented or corrected.

Phase I Inspections are not intended to provide detailed hydrologic and hydraulic analyses. In accordance with the established Guidelines, the Spillway Test Flood is based on the estimated "Probable Maximum Flood" for the region (greatest reasonably possible storm runoff), or fractions thereof. Because of the magnitude and rarity of such a storm event a finding that a spillway will not pass the Test Flood should not be interpreted as necessarily posing a highly inadequate condition. The Test Flood provides a measure of relative spillway capacity and serves as an aid in determining the need for more detailed hydrologic and hydraulic studies, considering the size of the dam, its general condition and the downstream damage potential.

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PHASE I INSPECTION REPORT
NATIONAL DAM SAFETY PROGRAM

Name of Dam:	Conewango Creek Watershed Davis Brook Dam (Site 1)
State Located:	New York
County Located:	Cattaraugus
Stream:	Davis Brook
Basin:	Allegheny River
Date of Inspection:	April 3, 1981

ASSESSMENT

Examination of available documents and visual inspection of Conewango Creek Watershed Davis Brook Dam (Site 1) and appurtenant structures did not reveal conditions which constitute a hazard to human life or property. However, the dam has some deficiencies which require further investigation and remedial action.

A wet condition of unknown cause was observed on the lower portion of the left downstream slope. It is recommended that the services of a qualified registered professional engineer be retained to evaluate this condition.

Using the Corps of Engineers screening criteria for review of spillway adequacy, it has been determined that the dam would not be overtopped under full PMF conditions. The PMF routed through the reservoir required only 46 percent of the spillway outflow capacity. The spillway capacity is therefore judged as adequate.

The recommended investigation should be completed within 12 months of notification to owner, and remedial actions resulting from these investigations completed in the subsequent 12 months.

The following remedial measures should be performed within 1 year of notification to owner:

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- Implement a program of diligent and periodic maintenance,
- Remove trees and brush from slopes,
- Regrade and fill in the erosion gullies.
- Install ladder rungs on the riser.

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Robert J. Farrell, P.E.

New York No. 55983

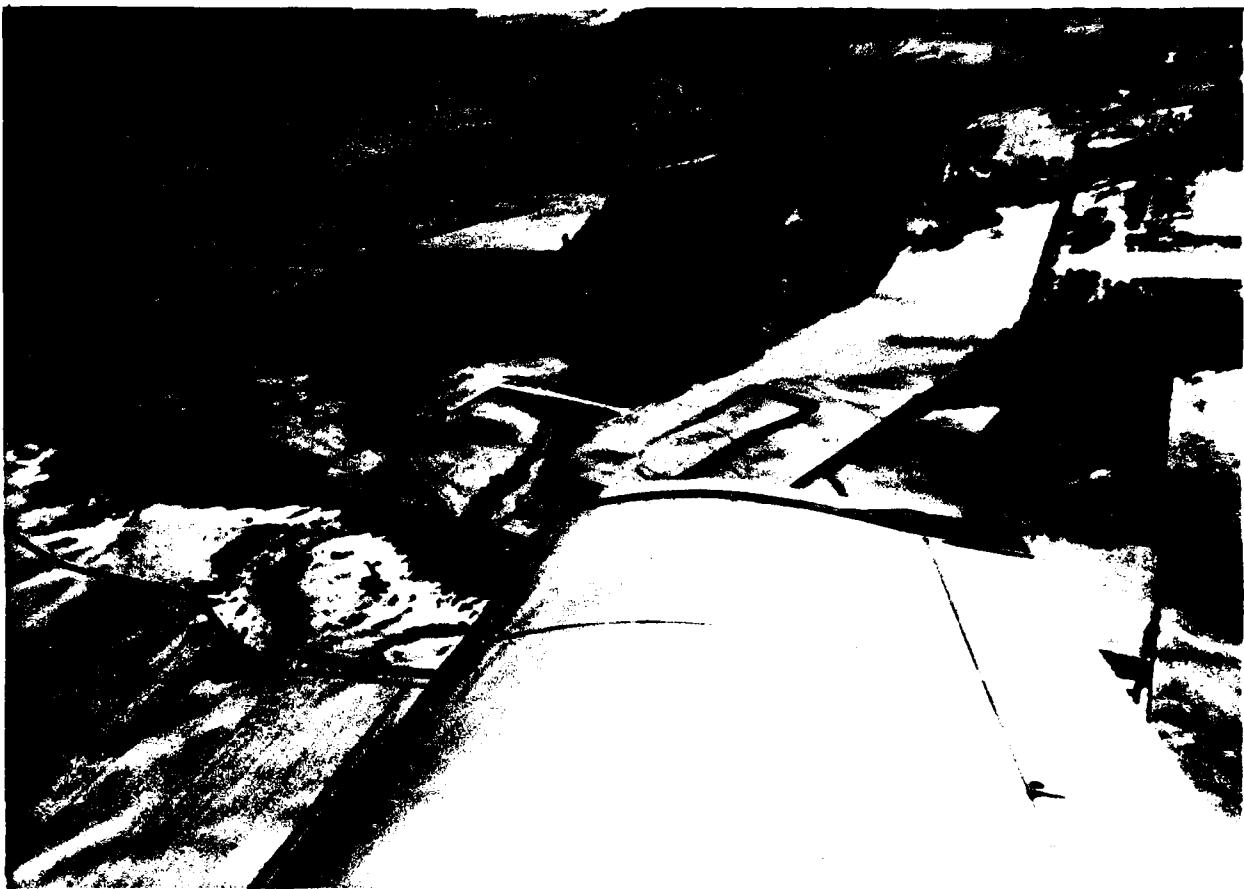
Col. W.M. Smith, Jr.
Col. W.M. Smith, Jr.
New York District Engineer

Approved by:

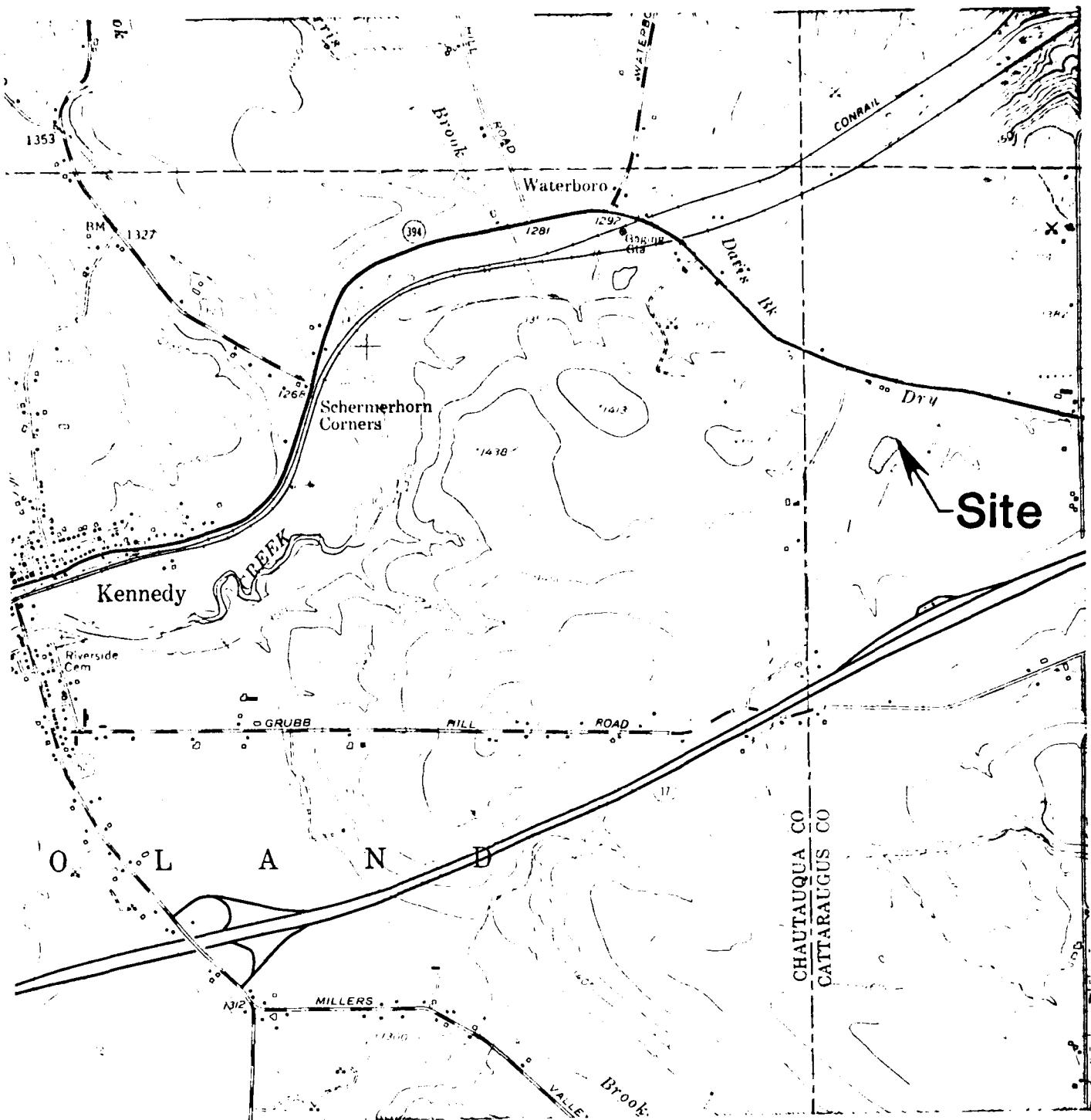
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Davis Brook Dam (Site 1)



AERIAL VIEW



Davis Brook Dam (Site 1)

LOCATION PLAN

Scale: 1-2000'

PHASE I INSPECTION REPORT
NATIONAL DAM SAFETY PROGRAM
CONEWANGO CREEK WATERSHED
DAVIS BROOK DAM (SITE 1)

SECTION I - PROJECT INFORMATION

1.1 GENERAL

a. Authority

The Phase I inspection reported herein was authorized by the New York District Corps of Engineers in a letter dated 24 February 1981, in fulfillment of the requirements of the National Dam Inspection Act, Public Law 92-367, dated 8 August 1972.

b. Purpose of Inspection

This inspection was conducted to evaluate the existing conditions of the dam, to identify deficiencies and hazardous conditions, to determine if these deficiencies constitute hazards to life and property, and to recommend remedial measures where required.

1.2 DESCRIPTION OF THE PROJECT

a. Location

The Davis Brook Dam is located approximately one-quarter mile east of the Chautauqua-Cattaraugus County line and approximately 800 ft. south of New York Rte 394. It can be reached from both New York Rt. 394 and Grubb Hill Road. The dam is approximately 2.5 miles east of Kennedy, New York and shown on U.S.G.S. Kennedy, New York quadrangle with coordinates approximately at N42° 09.7', W79° 03.4' (see location plan). Page B-4 of Appendix B is a site plan for this dam.

b. Description of Dam and Appurtenances

The dam consists of a zoned earthfill embankment with an earthfill cutoff trench below; a principal spillway with a reinforced concrete riser structure and outlet pipe; and a vegetated earth channel emergency spillway located at the right abutment. The length of the dam embankment is approximately 565 ft. The overall length of the dam is approximately 794 ft. including the emergency spillway which has a weir length of 200 ft.

1) Dam Embankment

The embankment consists of a zoned compacted earth structure of gravelly or silty sand and clayey silty gravelly sand. It is founded on glacial till. It is a maximum of 48 ft. high.

The upstream slope is 3 horizontal to 1 vertical and the downstream slope is 2.5 horizontal to 1 vertical. The crest width is 16 ft.

Beneath the embankment is an earthfill cutoff trench of variable width at the bottom. According to available plans it is constructed of the same material as the embankment.

2) Emergency Spillway

The emergency spillway is cut into sand and gravel in the right abutment. A diversion berm of compacted fill has been constructed on the east side with side slopes of 3 horizontal to 1 vertical. The grass covered channel curves around the east end of the dam embankment

The control section is 200 ft. wide and 30 ft. long and the downstream channel is roughly 250 ft. long.

3) Principle Spillway

The principle spillway consists of a reinforced concrete drop inlet structure with a sluice gate controlled inlet pipe, two uncontrolled orifice inlets and a 30 in. outlet pipe supported on a concrete cradle.

The inside dimensions of the riser structure are 32.25 ft. high and 7.5 ft. wide normal to the axis of the dam. It is 2.5 ft. long parallel to the embankment and flares to 14.2 ft. long at the top. The walls of the structure are 15 in. thick for the bottom 6 ft., 12 in. thick for the next 5 ft., and 10 in. thick for the top section. The top slab is 8 in. thick. The structure is founded on a 14 ft. by 15.5 ft. spread footing.

The "low stage inlet" is an uncontrolled opening approximately 16.3 ft. above the sluice gate invert. It is 16 in. wide and 12 in. high and is located in the upstream face of the riser structure. The water flows over this orifice and drops into the riser structure. It is protected by a trash rack assembly approximately 5.5 ft. high and 4.2 ft. wide. This assembly is fabricated from galvanized steel angle sections.

The "high stage inlet" consists of two openings approximately 30 ft. above the sluice gate invert. They are 7.5 ft. wide and 15 in. high and are located in the left and right sides of the flared portion of the riser structure. They are protected by a galvanized steel grating 25 in. high placed in front of each high stage opening and 5 galvanized steel angles placed in the sloping section below each opening. A 30 in. diameter manhole permits access into the riser structure.

The riser structure is drained by a 30 in. diameter reinforced concrete pressure pipe. It is approximately 224 ft. long and drops approximately 4.2 ft. over that length. The pipe penetrates the downstream side of the riser structure and is supported by a 7.5 in. thick concrete cradle within the embankment. Plans indicate 6 concrete anti-seep collars cast around the pipe within the embankment.

The downstream end of the conduit and cradle extend approximately 8 ft. downstream of the embankment. The pipe and bedding is supported by a reinforced concrete bent. The discharge conduit outlets into a stone revetted plunge pool.

4) Foundation and Embankment Drainage

A vertical seepage drain with graded filter is located in the downstream foundation at a variable distance downstream of the centerline of the dam. It extends the full length of the embankment. The drain is approximately 4 ft. wide and variable depth. For approximately 100 ft. either side of the principal spillway the drain includes a system of 8 in. diameter pipe which outlets to the left and right of the outlet conduit.

5) Reservoir Drain

The reservoir drain consists of a reinforced concrete inlet with an invert elevation of 1323.0 ft. (MSL). The inlet is drained by 42.0 ft. of 12 in. diameter cast iron pipe resting on a 4 in. thick unreinforced concrete cradle. The pipe enters the upstream side of the riser structure with an invert elevation of 1321.4 ft. (MSL), 1.0 ft. above the riser floor. The drain is regulated inside the riser structure by a 12 in. diameter slide gate, and a stem and pipe sleeve which rise to the wrench socket flush with the top slab of the riser, where a T-wrench handle may be inserted.

c) Size Classification

The dam's maximum height of 48 ft. places it in the INTERMEDIATE size category according to the Corps of Engineers' Recommended Guidelines.

d) Hazard Potential Classification

The hazard potential classification for this dam is HIGH because of the significant economic and high potential for loss of life downstream in the event of dam failure. Section 5 of this report presents more detailed discussion of the hazard potential.

e) Ownership

The dam is owned by Richard L. Shields
P.O. Box 224
Kennedy, New York 14747
Tele: (716) 267-4801

f) Operator

The dam is operated by:

Conewango Creek Watershed Commission
Donald Crowell, Chairman
RD #2
S. Dayton, New York 14138
Tele: (716) 988-3300

g) Purpose of Dam

The purpose of this dam is to reduce downstream flooding by providing temporary storage for the runoff from 1030 acres. The temporary storage is released gradually through the two-stage principal spillway system.

h) Design and Construction History

The dam was built under the Watershed Protection and Flood Prevention Act by the Conewango Creek Watershed Commission with the assistance of the Soil Conservation Service. It was completed in 1964.

i) Normal Operating Procedure

The dam is normally self-regulating.

1.3 Pertinent Data

a) Drainage Area

The drainage area for this dam covers 1.6 square miles. It is made up primarily of hilly woodland and pasture.

b) Discharge at Dam Site

1) Outlet Works

Normal discharge at the site is through the 30 in. diameter outlet pipe. In the event of severe flooding water would flow over the emergency spillway at elevation 1356.8 ft. (MSL). The invert of the low stage orifice is at elevation 1337.7 ft (MSL). The invert of the high stage orifice is at elevation 1351.4 ft. (MSL).

2) Maximum Known Flood

There is no data available for the maximum known flood at this dam site. Recent high water was observed at elevation 1347.5 ft. (MSL).

3) Ungated Spillway Capacity at Top of Dam

The capacity of the principal spillway with the reservoir at top of dam elevation 1361.6 ft. (MSL) is 165 cfs. The capacity of the emergency spillway is 6835 cfs at this level.

4) Ungated Spillway Capacity at Test Flood

The capacity of the principal spillway with the reservoir at test flood elevation (1359.7 ft. MSL) is 151 cfs. The capacity of the emergency spillway is 3103 cfs at this level.

5) Gated Spillway Capacity at Normal Pool

There are no gated spillways.

6) Gated Spillway Capacity at Test Flood

As previously mentioned, there are no gated spillways.

7) Total Spillway Capacity at Test Flood

The total spillway capacity at test flood elevation (1359.7 ft. MSL) is 3254 cfs.

c. Elevation (ft. above NGVD)

1) Streambed at toe of dam: 1313.4

2) Bottom of cutoff: variable, approximately 1312 minimum

3) Maximum tailwater - unknown, outlet conduit invert 1316.2

4) Normal pool: 1337.7

5) Full flood control pool: 1356.8

6) Spillway crest - Pond Drain Invert: 1323.0

Low level orifice: 1337.7

High level orifice: 1351.4

Emergency spillways: 1356.8

7) Design surcharge (original design): 1358.9

8) Top of dam: 1361.6

9) Test flood surcharge: 1359.7

d. Reservoir (Length in feet)

- 1) Length of maximum pool: 2100⁺ ft.
- 2) Length of normal pool: 800⁺ ft.
- 3) Length of flood control pool: 2000⁺ ft.

e. Storage (acre-feet)

- 1) Normal pool: 23
- 2) Flood control pool: 175
- 3) Spillway crest pool:
 - a) Low stage inlet: 23
 - b) High stage inlet: 86
 - c) Emergency spillway: 175
- 4) Top of dam: 273
- 5) Test flood pool: 230

f. Reservoir Surface (acres)

- 1) Normal pool: 4
- 2) Flood control pool: 18
- 3) Spillway crest pool:
 - a) Low stage inlet: 4
 - b) High stage inlet: 14
 - c) Emergency spillway: 18
- 4) Test flood: 21
- 5) Top of dam: 23

g. Dam

- 1) Type: Earth Embankment
- 2) Length: 565
- 3) Height: 48 ft.
- 4) Top Width: 16 ft.
- 5) Side Slopes:

Upstream: 3H:1V
Downstream: 2.5H:1V
- 6) Zoning: Embankment of clayey, silty, gravelly sand with dual graded filter at downstream embankment seepage drain under full length of embankment
- 7) Impervious Core: Semi-pervious clayey silty gravelly sand
- 8) Cutoff: Variable width, earthfill
- 9) Grout Curtain: None

h. Diversion and Regulating Tunnel

Not applicable

i. Spillways

1. Type:

- a) Principal Spillway: Reinforced concrete drop inlet
- b) Emergency Spillway: Grass covered earth channel cut in right abutment

2. Length of Weir:

- a) Low Level Orifice: 16 inches
- b) High Level Orifice: 15 feet
- c) Emergency Spillway: 200 feet

3. Crest Elevation: (feet above NGVD)

- a) Low Level Orifice: 1337.7
- b) High Level Orifice: 1351.4
- c) Emergency Spillway: 1356.8

4. Gates: None

5. Upstream Channel: Davis Brook, narrow stream
to reservoir through farm and woodland

6. Downstream Channel: Davis Brook, narrow stream through
farm and woodland

j. Regulating Outlet:

None

SECTION 2 - ENGINEERING DATA

2.1 GEOLOGY

Bedrock at the dam site is upper Devonian Age (345-375 million years ago) known as the Canadaway Group. These relatively underformed and flat-lying sedimentary rocks consist of interbedded shales and siltstones. Regionally, the rock forms a homoclinal dipping southward to southwestward at approximately 40 feet per mile. Small terraces and low folds locally modify this dip to essentially flat-lying over short distances. Only minor folding and faulting are found in the region with no major or active faults known to exist in the area.

The Davis Brook Dam is in a region classified as Zone 2 seismicity, as shown in Figure No. 1 of the Recommended Guidelines for Safety Inspection of Dams.

Pleistocene glaciation (beginning approximately 2 million years ago) modified the topography by means of both erosion and deposition. The thick continental ice sheet, moving southward from Quebec and Ontario, advanced and receded repeatedly in the area smoothing terrain by glacial scour and mantling the uplands with till deposits.

The Pleistocene geology of the dam site is that of glacial ground moraine. Generally alluvial gravels overlay dense sandy glacial till at the site. The till tends to be sparsely to moderately stony and very impermeable. In recent times, alluvium eroded from uplands has been deposited on these glacial deposits.

2.2 SUBSURFACE INVESTIGATION

Test hole logs are contained in the "As-Built" drawings; however, the copies are illegible and are not included in Appendix B.

2.3 DESIGN RECORDS

The records available for the project consists of 18 contract drawings which show the plans, sections and details for the dam, appurtenant structures, fencing details, and logs of test holes; and a design report issued by the U.S. Soil Conservation Service dated May 1969.

2.4 CONSTRUCTION RECORDS

Construction records and specifications are available at the U.S. Soil Conservation Service, Design Section, Syracuse, N.Y.

2.5 OPERATION RECORDS

No written maintenance or operation records exist for the dam.

2.6 EVALUATION OF DATA

Information obtained from the "As-Built" drawings is consistent with observations made during this inspection. The information obtained from available data was considered adequate for the Phase I inspection and evaluation.

SECTION 3 - VISUAL INSPECTION

3.1 Findings

a. General

The Davis Brook Dam is in GOOD condition at the present time.

b. Dam

1) Earth Embankment (See Photos 1, 5, 6, and 8)

The grass growth is heavy on this embankment impeding inspection of the slopes. Shrubs were noted along the right upstream abutment contact and to the right of the intake structure on the upstream slope.

Erosion gullies 1 to 2 in. wide and 1 in. deep were noted in the right downstream abutment contact.

The crest of the dam is in good condition.

There is no slope protection on the upstream slope other than the vegetative cover. Approximately 6 to 8 in. of erosion due to wave action was noted at and above the water line on the upstream slope.

The toe drain under the downstream slope shows no flow emanating from its outlets. The downstream left slope is wet over the bottom 15 ft. This may be the result of seepage or natural groundwater from the abutment. No staining was observed.

Animal burrows were noted in the right upstream and downstream slopes.

2) Emergency Spillway (See Photos 6, 7, and 8)

This spillway is in good condition. Some wet areas were noted but they are the result of natural groundwater or ponded runoff. Some debris was noted in the channel and should be cleared.

c. Appurtenant Structures

1) Drop Inlet Service Spillway (See Photos 1 and 2)

The structure is in good condition with no evidence of spalling, cracking, or efflorescence. The trash racks are in good condition, and free from debris accumulation.

2) Pond Drain Inlet Pipe

At the time of inspection, the 12 in. pond drain inlet was completely submerged and could not be observed.

d) Reservoir Area (See photos 5 and 8)

The shore of the reservoir is generally shallow sloping pasture or woodland. It appears to be stable and in good condition.

e) Downstream Channel (See photo 4)

The downstream channel is a narrow channel passing over relatively flat flood plain. There is rip rap protection of the plunge pool. Some erosion of the right bank has taken place downstream of the plunge pool.

3.2 Evaluation

The dam is generally in good condition. The potential problems noted during the visual inspection are listed below.

- a) The wet area noted over the bottom 15 ft. on the downstream left slope.
- b) Drainage gullies along the right downstream abutment.
- c) Animal burrows on the right upstream and downstream slopes.
- d) Debris on upstream slope and in the emergency spillway channel.
- e) Erosion of the downstream channel and the upstream slope of the dam at the waterline.
- f) Brush growing on the upstream slope and the right abutment contact.
- g) Operation of the drain gate could not be checked due to its inaccessibility.

SECTION 4 - OPERATION AND MAINTEANCE PROCEDURES

4.1 PROCEDURES

No written operation and maintenance procedures exist for the project. The normal operation of the project consists of allowing water to flow through the service spillway outlet pipe.

4.2 MAINTENANCE OF DAM

It is reported that maintenance of the dam is performed when the need arises. Maintenance is considered adequate.

4.3 WARNING SYSTEM IN EFFECT

No warning system is in effect or in preparation.

4.4 EVALUATION

The overall condition of the dam and appurtenant structures appears to be good. Recommendations in connection with regular maintenance are discussed in Section 7.

SECTION 5 - HYDRAULIC/HYDROLOGIC

5.1 Drainage Area Characteristics

Davis Brook Dam is located on Davis Brook, a tributary of Conewango Creek in the Allegheny River basin, and has a drainage area of 1.6 square miles. The dam is situated approximately 2.5 miles northwest of Kennedy New York. The topography of the watershed is hilly woodland and pastures.

5.2 Design Data

This dam was designed as a Class C structure in accordance with criteria established in Washington Engineering Memorandum SCS-27. Under this classification, the emergency spillway is designed for a rainfall equal to $P(100) + 0.26 [PMP-P(100)]$, while the freeboard pool is designed for the PMP rainfall.

The Soil Conservation Service (SCS) design calculations have been reviewed. The dam was designed to contain the runoff for the 100-year flood without discharging through the emergency spillway. The peak outflow is 126 cfs and the peak elevation is 1356.8 ft. (MSL). The SCS design allowed for a 50-year sediment accumulation with a storage of 23.3 acre-ft. The principal spillway consists of 30 in. diameter reinforced concrete water pipe and a 2.5 ft. x 7.5 ft. reinforced concrete riser with two 7.5 ft. x 15 in. openings with a crest elevation of 1351.4 ft. (MSL). The riser has a 1.0 ft. x 1.3 ft. orifice with a crest elevation of 1337.7 ft (MSL). The emergency spillway control cross section is 200 ft. wide, with side slopes of 3 horizontal to 1 vertical and a crest elevation of 1356.8 ft. (MSL). The dam crest elevation is 1361.6 ft. (MSL).

5.3 Analysis Criteria

The analysis of the spillway capacity of the dam and the storage of the reservoir was performed using the Corps of Engineers HEC-1 Dam Safety Version computer model. The unit hydrograph was defined by the Snyder Synthetic Unit Hydrograph method, and the Modified Puls routing procedure was incorporated. The Probable Maximum Precipitation (PMP) was 22.8 in. (24 hours 200 sq. miles) from Hydrometeorological Report #33 in accordance with the Recommended Guidelines of the Corps of Engineers. The dam is 48 ft. high and impounds approximately 273 acre-ft. at the top of the dam. The dam is classified as a HIGH hazard and INTERMEDIATE in size, according to the Recommended Guidelines of the Corps of Engineers. The spillway design flood is the Probable Maximum Flood (PMF). The floods selected for analysis were 20, 40, 50, 60, 80 and 100% of the PMF flows. The PMF inflow of 3261 cfs was routed through the reservoir and the peak outflow was determined to be 3254 cfs. The peak PMF outflow would produce a velocity of 7.0 ft./sec. on the emergency spillway and should not create an erosion problem.

5.4 Reservoir Capacity

The reservoir capacities at the crest of the emergency spillway and at the top of the dam are 175 acre-ft. and 273 acre-ft., respectively. Surcharge storage between the emergency spillway crest and the top of dam is equivalent to 1.1 in. of runoff from the drainage area.

5.5 Experience Data

There are no flood records for the dam site, however, during the field investigation, evidence of recent high water was observed at elevation 1347.5 ft. (MSL). This reservoir elevation corresponds to a peak outflow of 16 cfs.

5.6 Overtopping Potential

The maximum capacity of the spillways is 7000 cfs which is greater than the PMF peak outflow of 3254 cfs. The dam is not overtapped by the PMF, the peak elevation being 1.9 ft. below the top of the dam.

5.7 Analysis of Downstream Impacts

During the field investigation, dwellings and highways located downstream of the dam were identified and referenced to the channel invert. The cross section locations used in the downstream channel routing are shown on Page D-2, Appendix D. The impacts of the PMF on dwellings located downstream of the dam are shown in Table 5.1. For the purposes of this analysis, a danger of loss of life was assumed to exist if the computed PMF water surface was above the first floor elevation of a structure. This situation does not occur at any of the structures and no roads are overtapped during the PMF. In spite of these results, the potential danger of loss of life and economic damage is substantial enough to warrant classification as a HIGH hazard dam.

5.8 Evaluation

The spillway of Davis Brook Dam will safely pass the PMF without overtapping, and is therefore assessed as "Adequate". Potential problems include:

- a) The danger of loss of life and economic damage downstream of the dam for the test flood conditions.

TABLE 5.1
SUMMARY OF DOWNSTREAM IMPACTS FOR PMF

<u>Location #</u> <u>(see page D-2 Appendix D)</u>	<u>Location</u>	<u># of Dwellings</u>	<u>Structure Height above Streambed*</u> <u>(ft)</u>	<u>Peak Flow (cfs)</u>	<u>Peak Stage (ft)</u>	<u>Comments</u>
			<u>(ft)</u>	<u>(cfs)</u>	<u>(ft)</u>	
1	1600' d/s of dam	1	14	3254	6	
2	1100' d/s Location #1	2	12	3251	8	
3	1600' d/s of Location #2	1 house 1 trailer	12.7 9.6	3246 3246	8 8	
4	500' d/s of Location #3	1	11.1 7.7	3246 3246	7 7	

*The structure height above the streambed is the difference between the first floor elevation and the channel invert.

SECTION 6 STRUCTURAL STABILITY

6.1 Visual Observations

There does not appear to be significant displacement or distress associated with the embankments at this site. The dam appears to be in good condition at the present time.

6.2 Design and Construction Data

Analyses carried out by the Soil Conservation Service during the design and construction phase included slope stability analyses by the infinite slope and Swedish circle methods. The soil parameters assumed for the final analysis were: Relative density 97%, $\phi = 31.5^\circ$ and $c = 675$ psf. Based on these assumptions, the factors for safety were higher than 2.5 for both upstream and downstream slopes. The dam is therefore considered to have adequate factors of safety for stability.

6.3 Post Construction Changes

There have been no known changes to any of the embankments or structures at this dam.

6.4 Seismic Stability

The dam is located in Seismic Zone No. 2 and, in accordance with the recommended Phase I guidelines, a seismic stability analysis is not warranted.

SECTION 7 - ASSESSMENT/RECOMMENDATIONS

7.1 ASSESSMENT

a. Safety

Examination of the available documents and visual inspections of the Conewango Creek Watershed Davis Brook Dam (Site 1) and appurtenant structures did not reveal any conditions which constitute a hazard to human life or property. The dam and its appurtenances are considered to be in good condition at the present time.

Using the Corps of Engineers screening criteria for review of spillway adequacy, it has been determined that the dam would not be overtopped for the spilway design flood of the full PMF nor for one-half the PMF. The principal and auxiliary spillway capacity are, therefore, judged as adequate.

b. Adequacy of Information

This report and its conclusions are based on visual inspection, interview data, contract drawings, and office hydrologic/hydraulic studies. This information and data are adequate for a Phase I inspection.

c. Need for Additional Investigations

It is recommended that the services of a qualified registered professional engineer be retained to evaluate the wet condition observed on the lower portion of the left downstream slope.

The engineer should make recommendations for remedial measure if warranted and the owner should implement the findings of these studies.

d. Urgency

The recommended investigation should be completed within 12 months of notification to owner and remedial actions resulting from these investigations completed in the subsequent 12 months. The remedial measures or actions listed below should be completed within one year from notification to owner.

7.2 RECOMMENDED MEASURES

It is recommended that the owner institute the following remedial measures:

- 1) Develop a formal written downstream warning system to alert the appropriate officials and residents in the event of an emergency.
- 2) Develop and maintain a program of periodic technical inspections.

- 3) Implement a program of diligent and periodic maintenance including but not limited to: mowing of slopes and spillway channels; backfilling ruts, drainage gullies, and animal burrows with suitable compacted material; clearing debris from track racks and upstream slopes; and checking the operability of the drain gate.
- 4) Remove trees and brush from slopes including the roots. The resulting voids should be backfilled with suitable compacted material.
- 5) Regrade and fill in the erosion gullies on the downstream right slope and reseed the disturbed areas.
- 6) Install ladder rungs on the riser to provide access to the drain gate housing.

APPENDIX A
VISUAL INSPECTION CHECKLIST

VISUAL INSPECTION CHECKLIST

1) Basic Data

a. General

Name of Dam Davis Brook Dam
Fed. I.D. # NY 00564 DEC Dam No. 8B-3805
River Basin Allegheny
Location: Town Randolph County Cattaraugus
Stream Name Tributary of Davis Brook
Tributary of Conewango Creek
Latitude (N) 42° 09.7' Longitude (W) 79° 03.4'
Type of Dam Earth Embankment
Hazard Category High
Date(s) of Inspection April 3, 1981
Weather Conditions Sunny, 70°
Reservoir Level at Time of Inspection Approximately elevation 1338.2 ft.

b. Inspection Personnel Mr. James Reynolds, Mr. Jeff Hardin, Mr. Bob Farrell,
Mr. Ken Avery

c. Persons Contacted (including Address & Phone No.)
U.S. Soil Conservation Service Rm 771-Federal Bldg., 100 So. Clinton St., Syracuse, NY
State Construction Eng: Philip "Skip" Nelson 1-315-423-5502
Area 1 Proj. Engr. (Batavia): Pete Wright 1-716-343-3364
Contracting Ofc. (Conewango Creek Commission) Dick Shields 1-716-267-4801

d. History:

Date Constructed 1971 Date(s) Reconstructed _____

Designer U.S.D.A. Soil Conservation Service

Constructed by _____

Owner _____

Embankment

a. Characteristics

- (1) Embankment Material Gravelly or silty sand (SM) to clayey silt, gravelly sand (SC-SM) and (SP)
- (2) Cutoff Type Earthfill trench of variable bottom width
- (3) Impervious Core None
- (4) Internal Drainage System A dual graded filter makes up the downstream embankment, a 4 foot wide trench drain below the downstream embankment
- (5) Miscellaneous _____

b. Crest

- (1) Vertical Alignment Good
- (2) Horizontal Alignment Good
- (3) Surface Cracks None noted
- (4) Miscellaneous _____

c. Upstream Slope

- (1) Slope (Estimate) (V:H) 1 vertical to 3 horizontal
- (2) Undesirable Growth or Debris, Animal Burrows Brush growth approximately 30 feet right of intake structure, minor amounts of debris
- (3) Sloughing, Subsidence or Depressions None noted

(4) Slope Protection Vegetative cover and berm at water level 6 to 8 inches
of wave erosion at or just above the present water level

(5) Surface Cracks or Movement at Toe None noted

d. Downstream Slope

(1) Slope (Estimate - V:H) 1 vertical to 2.5 horizontal

(2) Undesirable Growth or Debris, Animal Burrows Burrows 40 feet from right
abutment 6 feet below crest (6" diameter), two more down slope

(3) Sloughing, Subsidence, or Depressions None noted

(4) Surface Cracks or Movement at Toe None noted

(5) Seepage Bottom 15 feet of left downstream slope is wet. This may be seepage
or natural groundwater from the abutment, no flow could be discerned. No
flow from toe drain outlets

(6) External Drainage System (Ditches, Trenches, Blanket) None noted

(7) Condition Around Outlet Structure Good

(8) Seepage Beyond Toe None noted

e. Abutments - Embankment Contact

A 6' x 6' slough has occurred approximately 12 feet below the crest at the left
upstream contact. Heavy brush at right upstream contact

(1) Erosion at Contact None noted other than slough at left upstream contact

(2) Seepage Along Contact None noted other than seepage at left downstream slope
discussed at 2-d-5

3) Drainage System

(a) Description of System 4 ft. wide trench drain containing a system of 8 in. diameter perforated pipe exiting on either side of the principal spillway outlet conduit

(b) Condition of System No flow was observed from the system

(c) Discharge from Drainage System None noted

4) Instrumentation (Monumentation/Surveys, Observation Wells, Weirs, Piczometers, etc.) None installed

5) Reservoir

a. Slopes Appear stable and in good condition

b. Sedimentation Very minor accumulation

c. Unusual Conditions Which Affect Dam None noted

6) Area Downstream of Dam

a. Downstream Hazard (No. of homes, highways, etc) Refer to Table 5.1

b. Seepage, unusual growth None noted

c. Evidence of movement beyond toe of Dam None noted

d. Conditions of Downstream Channel Small Slough on downstream right bank, approximately 20 ft. downstream of plunge pool

7) Spillway(s) (including Discharge Conveyance Channel)

a. General Good

b. Condition of Service Spillway Good, no evidence of cracking, spalling or efflorescence

c. Condition of Emergency Spillway Generally good; needs mowing and clearing of debris

d. Condition of Discharge Conveyance Channel Good

8) Reservoir Drain/Outlet

Type: Pipe Conduit _____ Other _____

Material: Concrete _____ Metal _____ Other Cast Iron

Size: 12" I.D. Length 42' (from dwgs)

Invert Elevations: Entrance 252 ft. Exit 252 ft.

Physical Condition (Describe): Unobservable

Material: _____

Joints: _____ Alignment _____

Structural Integrity: _____

Hydraulic Capability: _____

Means of Control: Gate _____ Valve Uncontrolled _____

Operation: Operable _____ Inoperable Other _____

Present Condition (Describe): Could not be operated due to missing handle.

9) Structural

- a. Concrete Surfaces _____ N/A

- b. Structural Cracking _____ N/A

- c. Movement - Horizontal & Vertical Alignment (Settlement) _____ N/A

- d. Junctions with Abutments or Embankments _____ N/A

- e. Drains - Foundation, Joint, Face _____ N/A

- f. Water Passages, Conduits, Sluices _____ N/A

- g. Seepage or Leakage _____ N/A

- h. Joints - Construction, etc. _____ N/A

- i. Foundation _____ N/A

- j. Abutments _____ N/A

- k. Control Gates _____ N/A

- l. Approach & Outlet Channels _____ N/A

m. Energy Dissipators (Plunge Pool, etc) _____ N/A

n. Intake Structures _____ N/A

o. Stability _____ N/A

p. Miscellaneous _____ N/A

10) Appurtenant Structures (Power House, Lock, Gatchouse, Other)

a. Description and Condition None

APPENDIX B

ENGINEERING DATA

APPENDIX B

<u>TITLE</u>	<u>PAGE</u>
Cover Sheet	B-2
Plan of Storage Area	B-3
Plan of Structural Works	B-4
Cut-Off Trench Excavation	B-5
Emergency Spillway	B-6
Fill Placement & Principal Spillway-Excavation	B-7
Drainage System	B-8
Drainage System	B-9
Plan Profile of Principal Spillway	B-10
Riser Structural Details	B-11
Riser Structural Details	B-12
Riser Structural Details	B-13
Riser Structural Details	B-14
Riser Trash Racks	B-15
Conduit Details	B-16
Reservoir Drain Inlet Details	B-17

CONEWANGO CREEK WATERSHED FLOODWATER RETARDING DAM SITE I

DRAINAGE AREA
FLOOD STORAGE
(TO EMERGENCY SPILLWAY TRENCH)
WATER SURFACE AREA
(SEDIMENT POOL)
HEIGHT OF DAM
VOLUME OF FILL

54,5
61,3

BUILT UNDER THE WATERSHED PROTECTION
FLOOD PREVENTION ACT
BY
CONEWANGO CREEK WATERSHED COMM.
WITH THE ASSISTANCE OF THE
SOIL CONSERVATION SERVICE
OF THE
U.S. DEPARTMENT OF AGRICULTURE

INDEX

SHEET 1	COVER SHEET
SHEET 2	PLAN OF STORAGE AREA
SHEET 3	PLAN OF STRUCTURAL WORKS
SHEET 4	CUTOFF TRENCH EXCAVATION
SHEET 5	EMERGENCY SPILLWAY
SHEET 6	FILL PLACEMENT AND PRINCIPAL SPILLWAY EXCAVATION
SHEET 7	DRAINAGE SYSTEM
SHEET 8	DRAINAGE SYSTEM
SHEET 9	PLAN PROFILE OF PRINCIPAL SPILLWAY
SHEET 10	RISER STRUCTURAL DETAILS
SHEET 11	RISER STRUCTURAL DETAILS
SHEET 12	RISER STRUCTURAL DETAILS
SHEET 13	RISER STRUCTURAL DETAILS
SHEET 14	RISER TRASH RACKS
SHEET 15	CONDUIT DETAILS
SHEET 16	RESERVOIR DRAIN INLET DETAILS
SHEET 17	FENCING DETAILS
SHEET 18	LOGS OF TEST HOLES
SHEET 19	LOGS OF TEST HOLES

ERSHED PROJECT

G DAM

1030 Acres
175 Ac Ft.

4 Acres

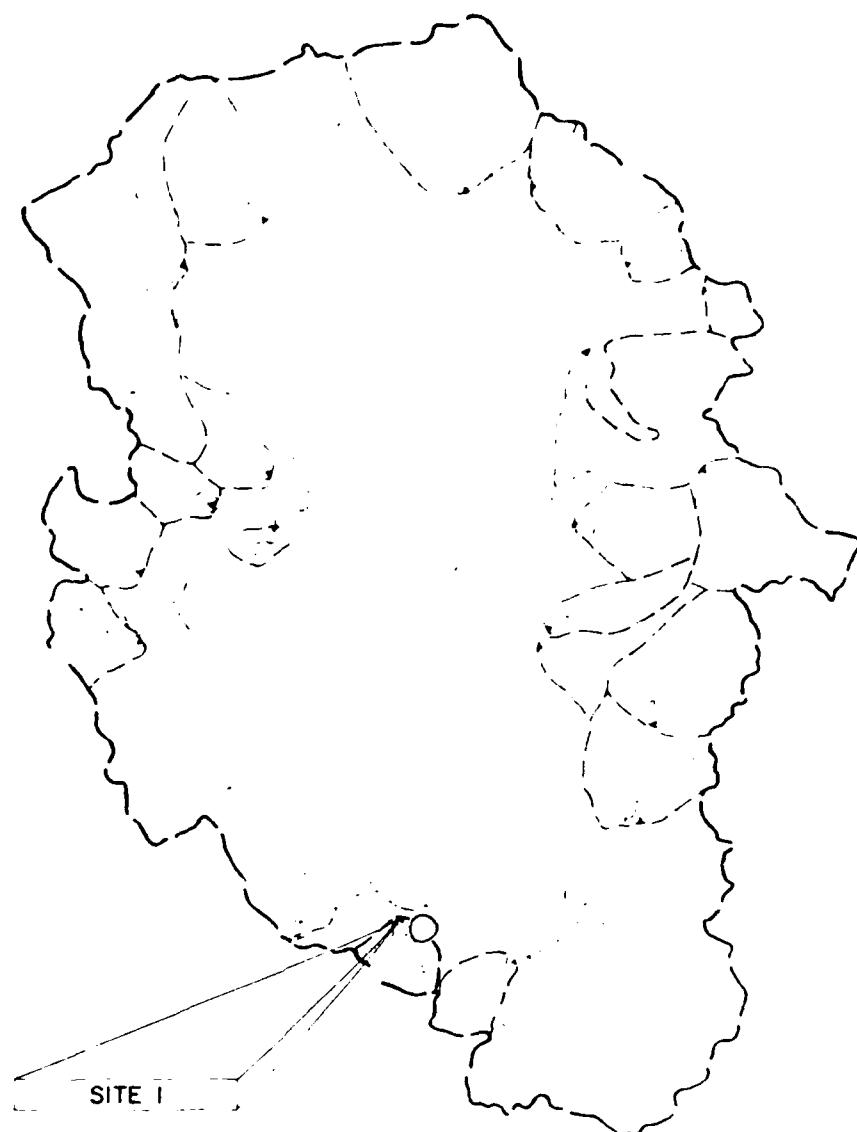
43 Feet
~~54,500~~ Cu Yds
61,361

ROTECTION AND
ACT

ED COMMISSION
F THE
VICE

ULTURE

OMMATION



4/17/77
AS BUILT

SITE I
FLOODWATER RETARDING DAM
CATTARAUGUS COUNTY, NEW YORK

ZOGRAFOS
J E POLULECH

3/69

B-2
2

CONSTRUCTION DETAILS

1. ALL AREA UPSTREAM AND OR DOWNSTREAM INCLUDE THE FOLLOWING:

✓ 1. EAST AREA OF DAM FL + 3 FEET EXTENSIONS BOTH UPSTREAM AND DOWNSTREAM FROM THE END OF DAM. ALSO FOUNDATION EXCAVATION ON LEFT ABUTMENT AS SHOWN ON SHEET 2

✓ 2. EAST AREA OF DIVE

✓ 3. THE END OF SPILLWAY INCLUDING 1 FEET OUTSIDE THE SLOPES AT A MAX. EXTEND 7 FEET WIDE OF SPILLWAY AT THE PUTBACK UP DOWN TO ELEV. 133.5 ✓

✓ AB BUTT

✓ LIMITS OF AREA TO BE CLEARED AND GRADED SHALL BE STAKED IN THE FIELD BY THE ENGINEER.

2. DEPTHS AND LIMITS OF MORROW EXCAVATION SHALL BE DETERMINED IN THE FIELD BY THE ENGINEER AS REQUIRED. SLOPING OF THE MORROW AREA SHALL BE NO STEEPER THAN 4 HORIZONTAL TO 1 VERTICAL.

3. AREAS UPSTREAM FROM DAM AND BELOW ELEVATION 134 ✓ SHALL BE CLEARED. LIMITS OF AREA TO BE CLARED SHALL BE STAKED IN THE FIELD BY THE ENGINEER.

4. OPTION SECTION OF MUD DUG TUNNEL TO BE COVERED WITH 1' OF TOP SOIL FROM STAL. 1366 TO APPROX. STAL. 1367 ✓

ELEV'S

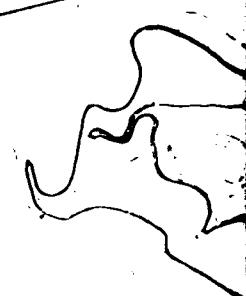
BM#3 1316.48

TBM#1 1329.75 Disk Nail - Cherry Tree

TBM#4 1366.46 Disk Nail - Cherry Tree
Fence Line 12" Truck
Right Abutment

TBM#5 1350.35 Disk - Nail - Elm Tree
Left Abutment -
Downstream From E Dam

70" STEEL PIPE
INV. # 13679

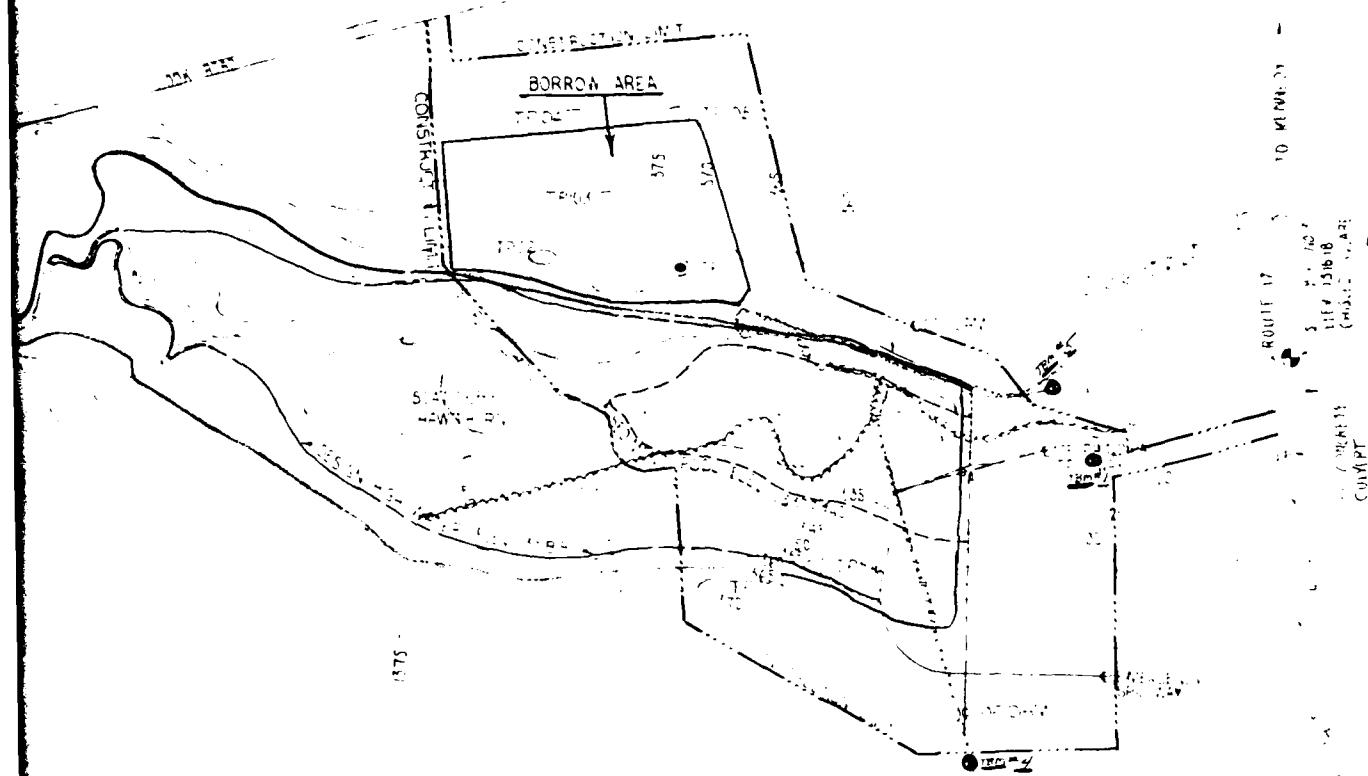


12-26-68
CONSTRUCTION

SITE 5 CONSTRUCTION

17-4-68

CONSTRUCTION



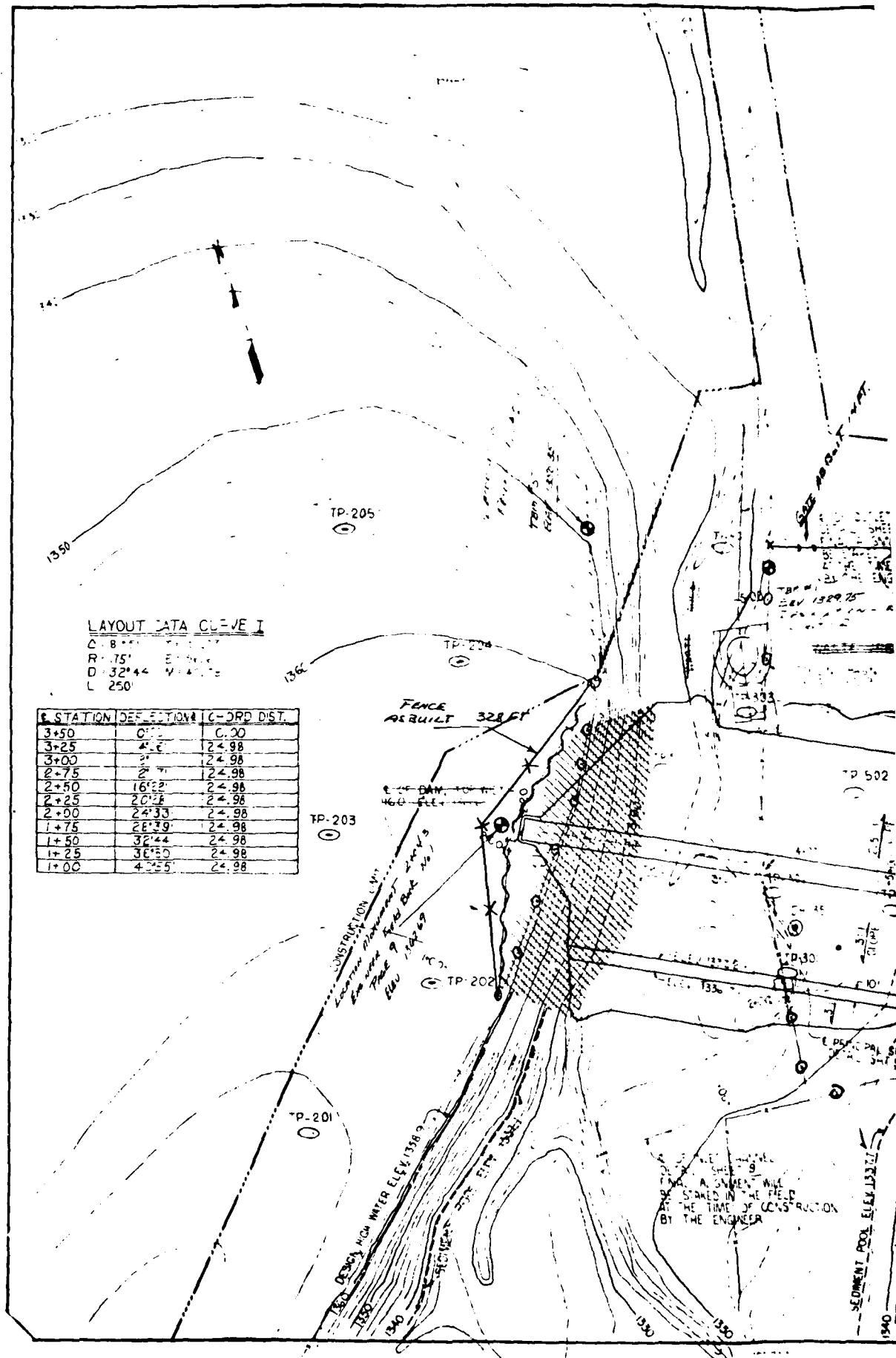
11/14/1971
AS BUILT

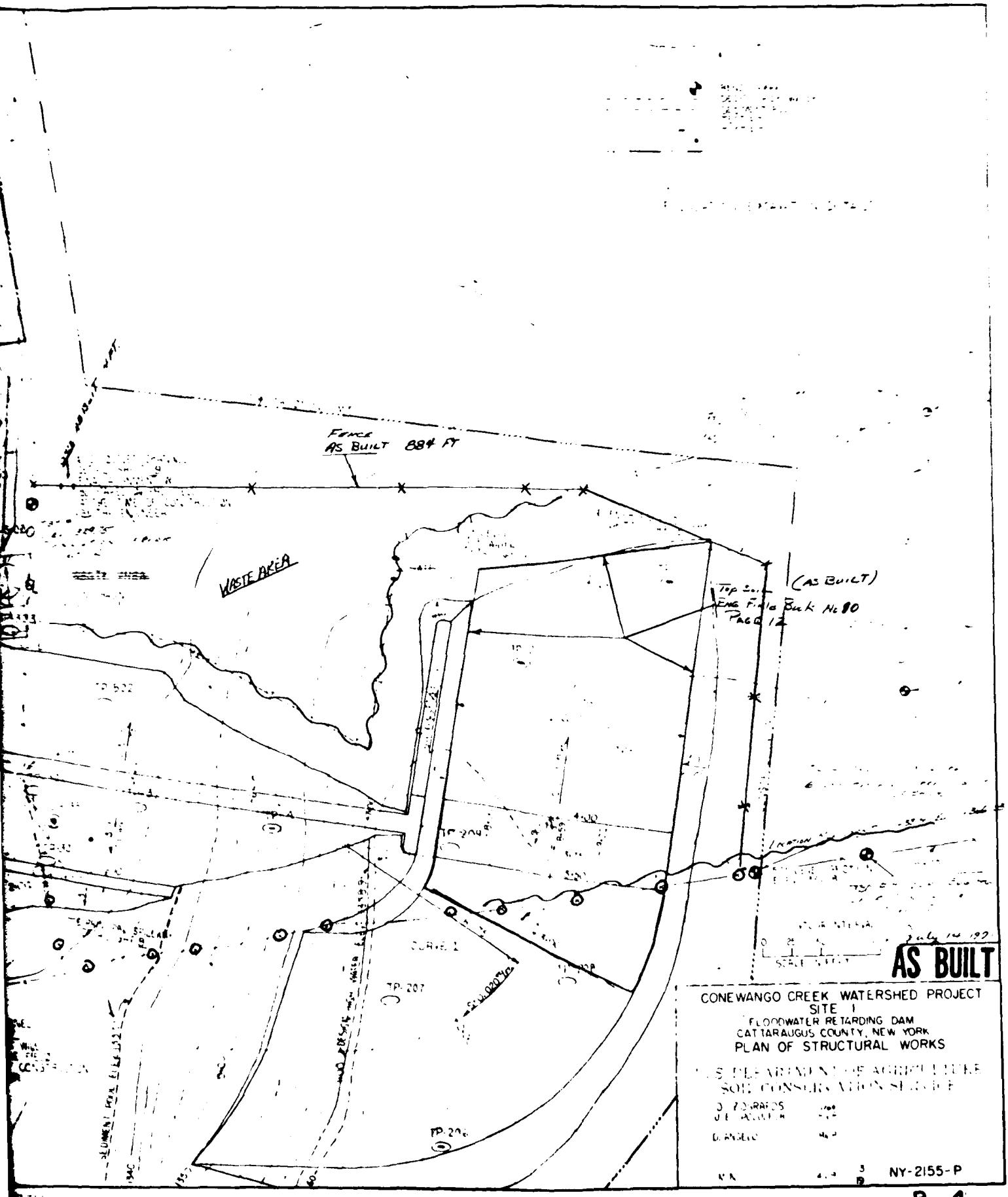
CONEWANGO CREEK WATERSHED
SITE 1
CONSTRUCTION
ROUTE 17 CONSTRUCTION
PLAN OF STORAGE AREA
U.S. DEPARTMENT OF AGRICULTURE
SOIL CONSERVATION SERVICE

J.E. POLULECH 8/68

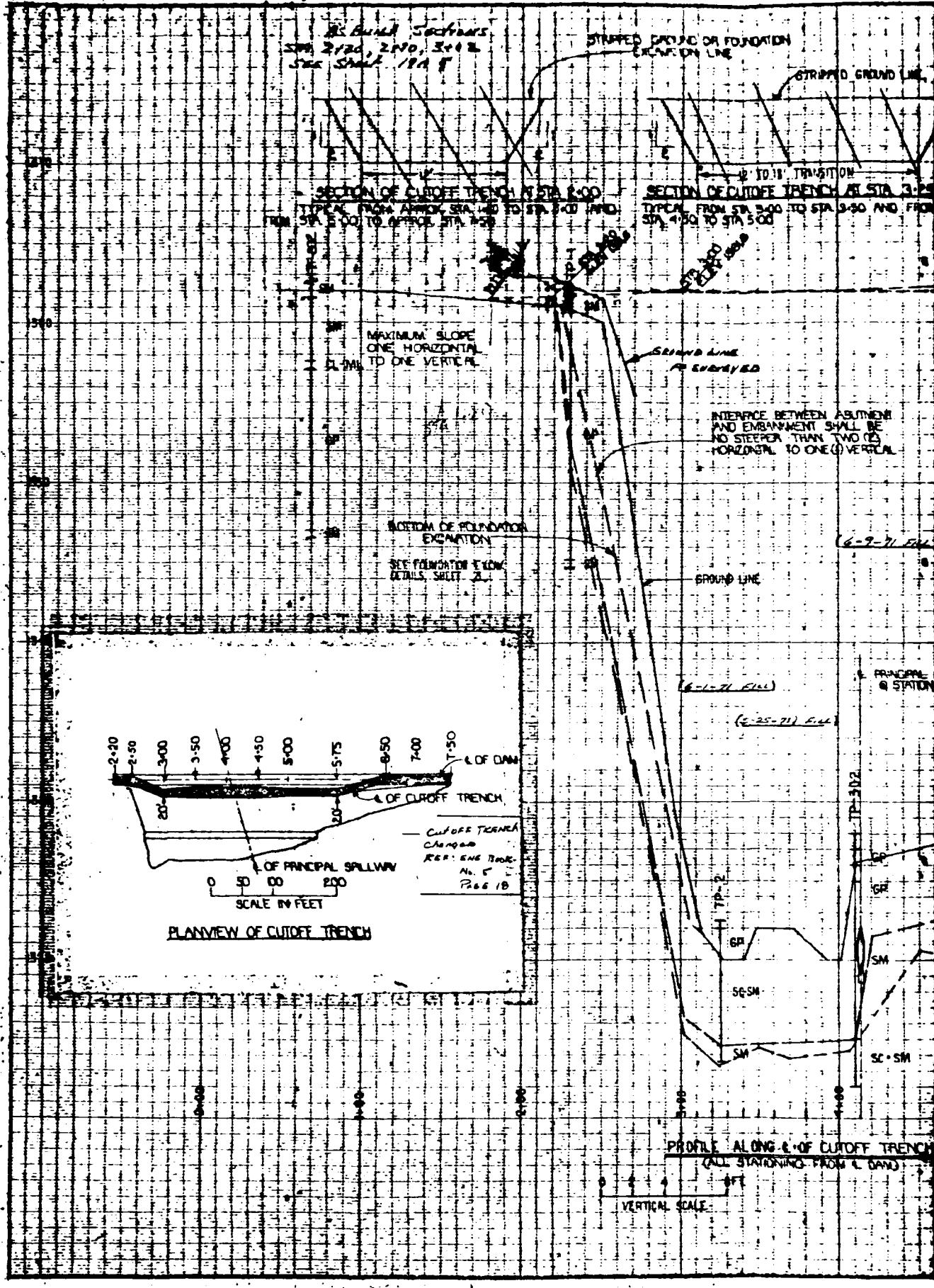
NY-2155 P

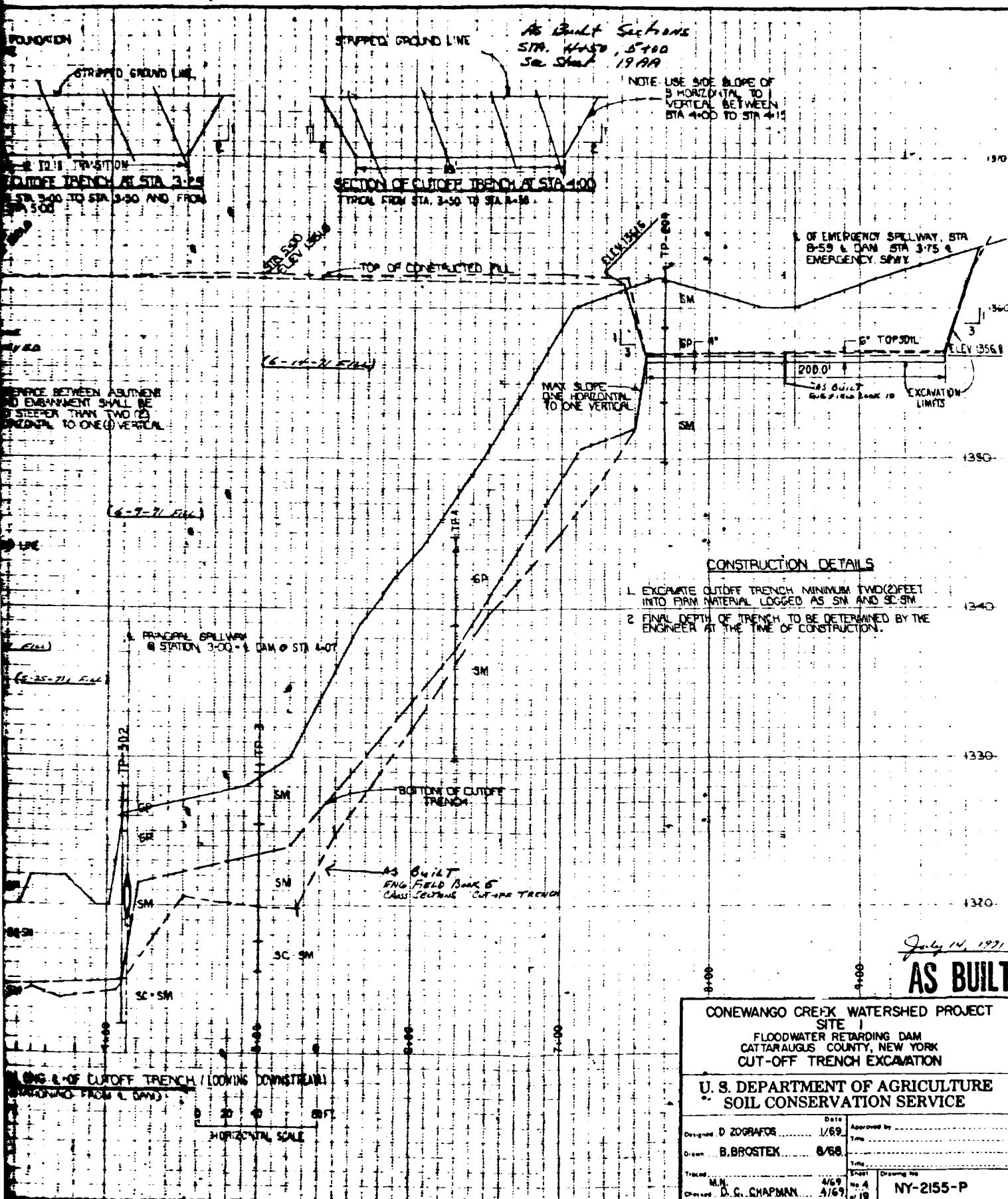
B-3

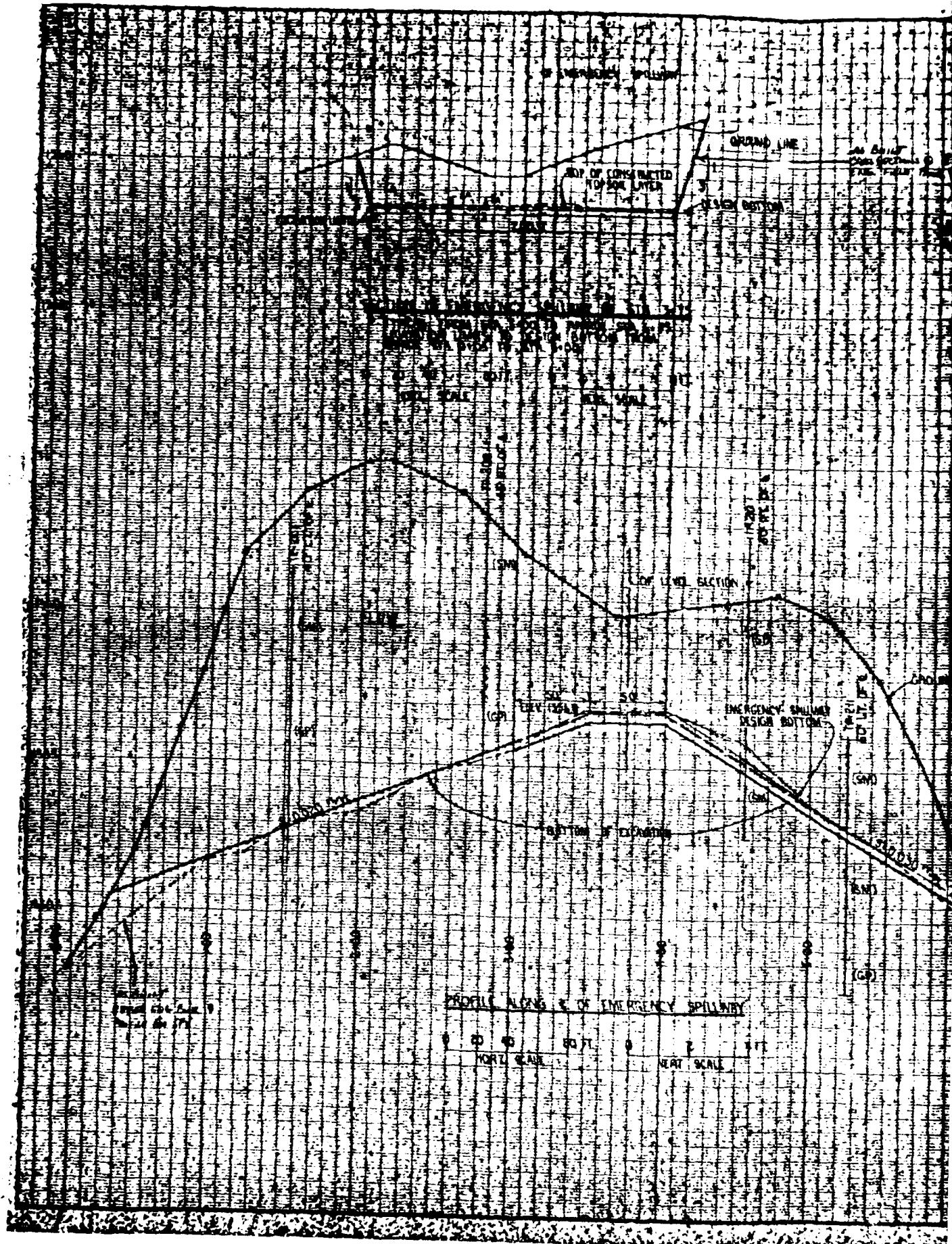




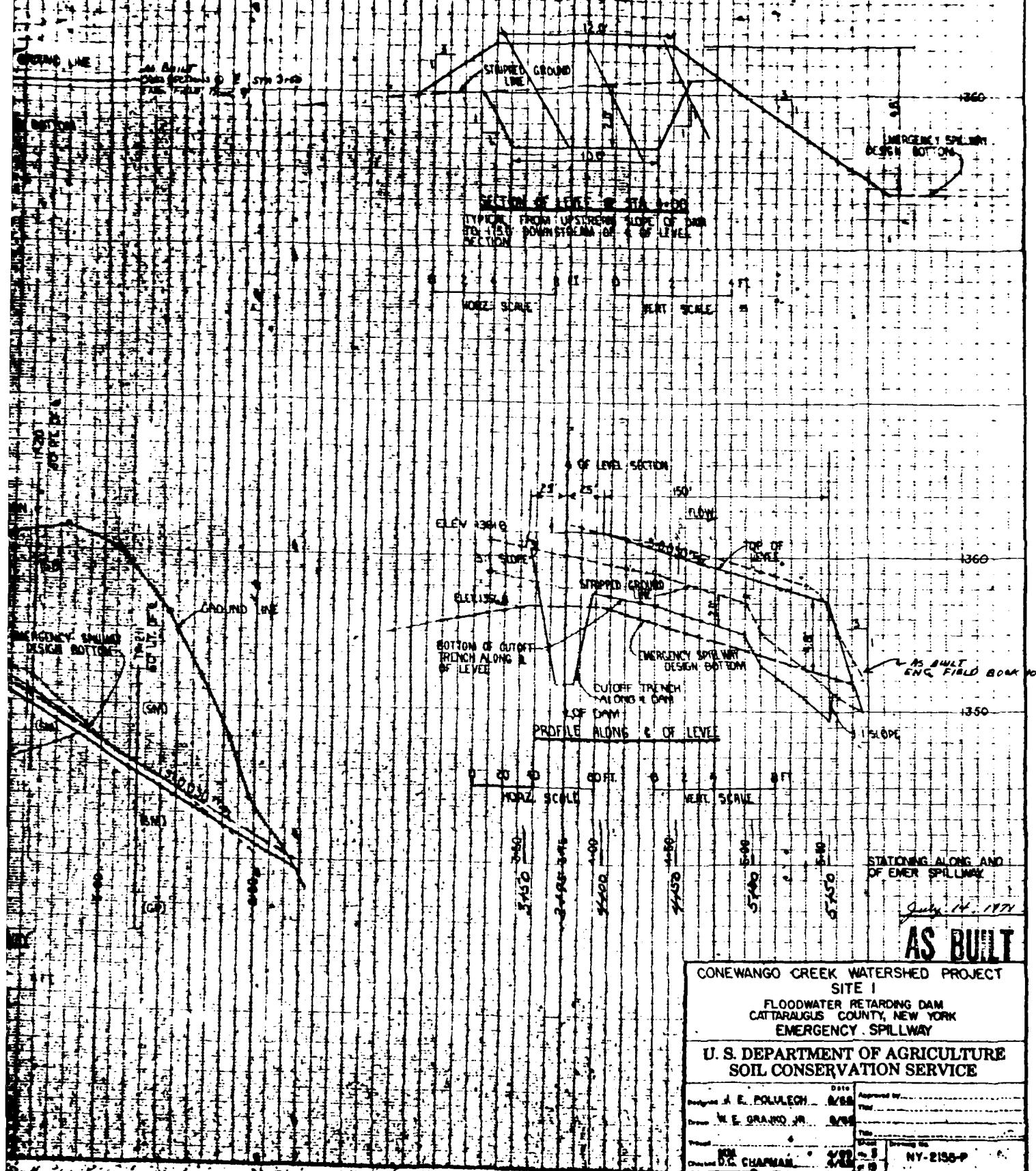
B - 4



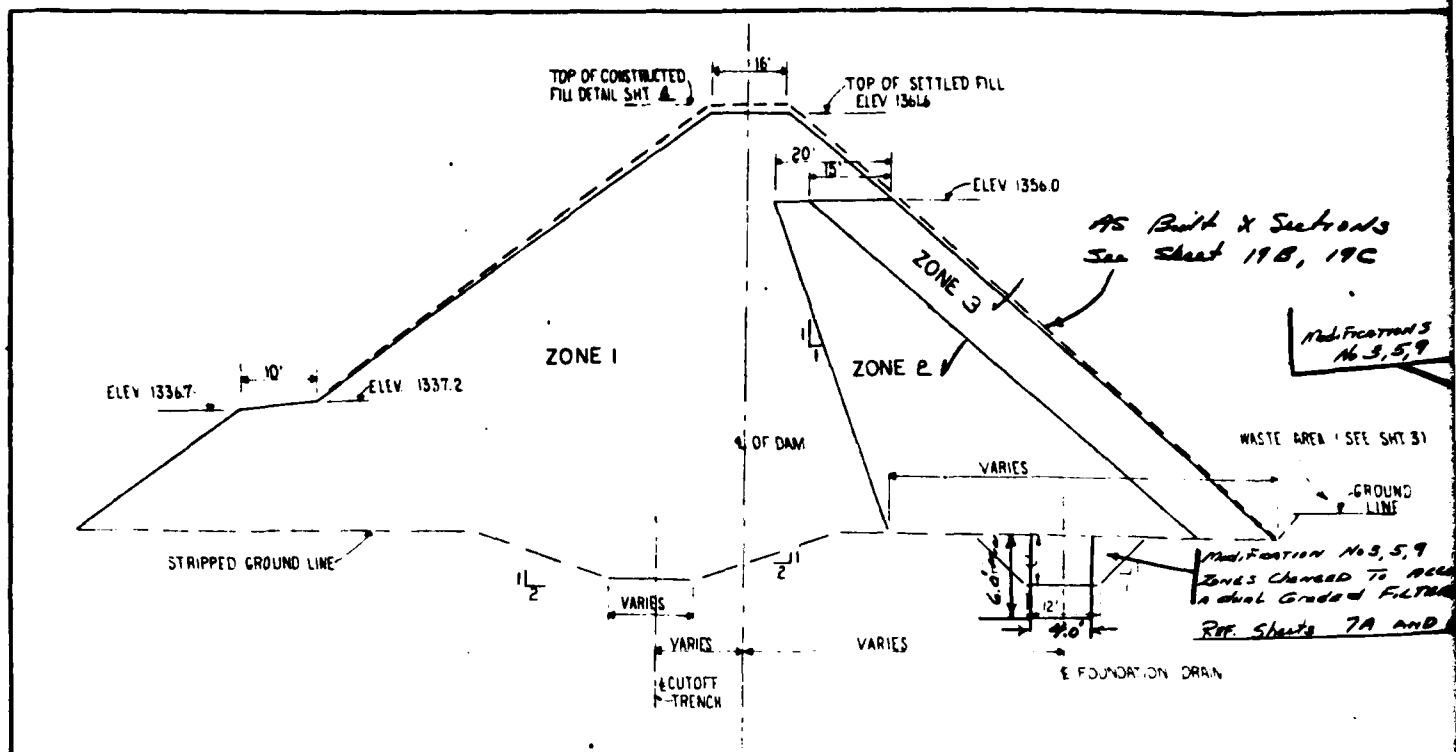




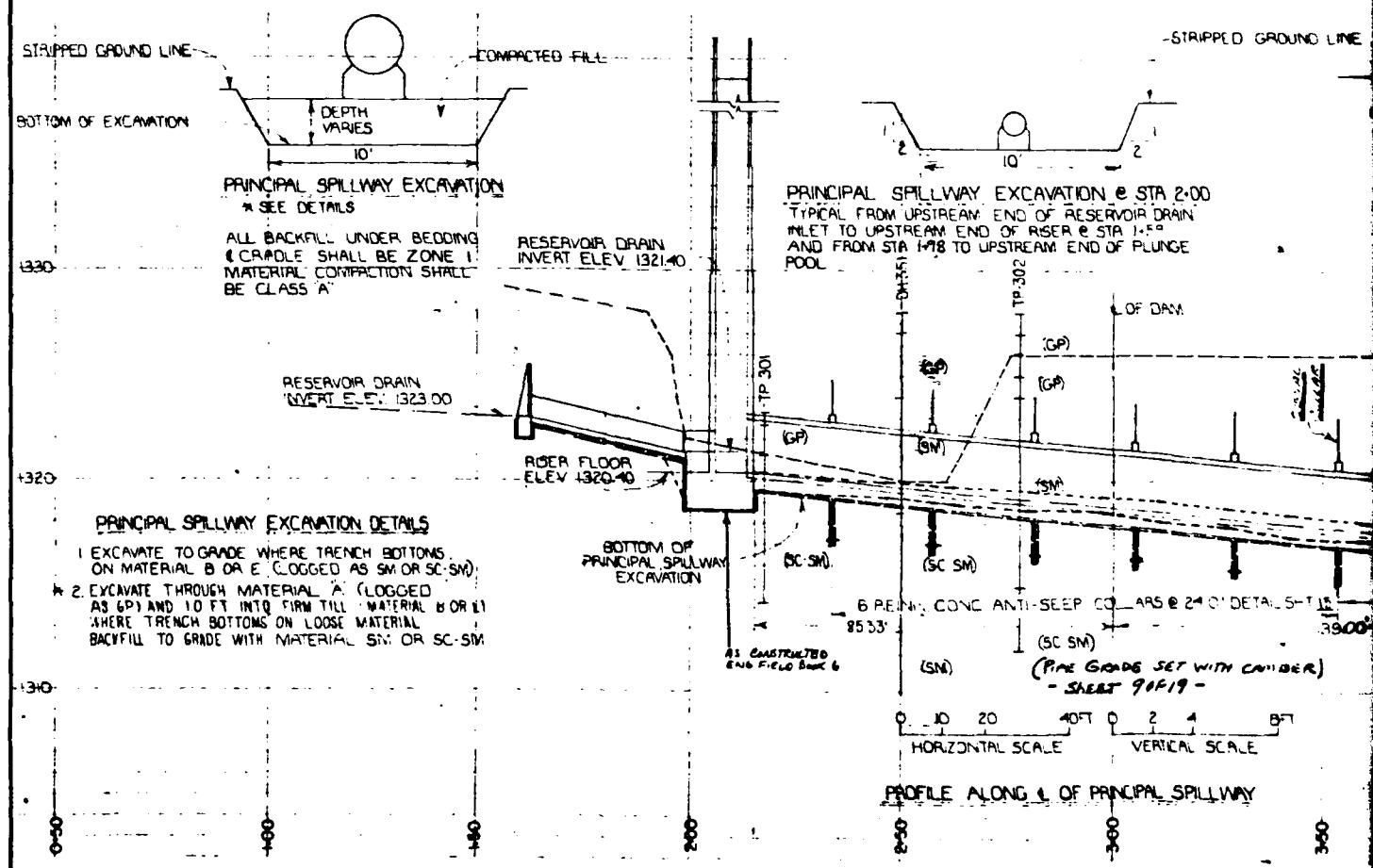
See Sheet 19D - A Built



B - 6



SECTION OF DAM AT STA 3:00
TYPICAL FROM APPROX STA 1:00 TO STA 7:58



ZONE	MATERIAL	EARTH FILL REQUIREMENTS			COMPACTOR S	CLASS	DEFINITION
		MAX ROCK SIZE 2	MAX. LIFT THICK 3	REQUIRED WATER CONTENT 4			
1	MATERIALS B, D, E, G AND H AS LABELLED ON SHEET 11 AND REPRESENTED BY TP 101 FROM 1 TO 12 TP 211 FROM 29 TO 13 TP 212 FROM 35 TO 8 TP 206 FROM 0.5 TO 27 TP 401 FROM 2 TO 5 TP 202 FROM 1.5 TO 5.5	6"	4"	WATER IN WET CONTENT SHAL. BE 2 PLACEMENT POINTS OF 100% OPT. W.	-	A	97% STD. DENSITY BASED ON ASTM D-698, METHOD A
2	MATERIAL "A" AS LABELLED ON SHEET 11 AND REPRESENTED BY TP 205 FROM 20-45	6"	9"	WET	V	SEE CONSTRUCTION SPECIFICATION 2	
3	SAME AS MATERIAL IN ZONE 2 PLUS OVERRSIZE REMOVED FROM ZONE 2	18"	27"	WET	V	SEE CONSTRUCTION SPECIFICATION 2	

WASTE AREA (SEE SHT 3)

-GROUND
LINE

Modification No. 3, 5, 9
ZONES CHANGED TO ALLOW
A dual Graded FILTER

REF. Sheets 7A AND 8A

IN DRAIN

- 1) THE PLACEMENT TABLE INDICATES THE PLACED SIZE OF MATERIAL.
- 2) MAXIMUM ROCK SIZE PLACED IN HAND COMPAKTED BACKFILL SHALL BE 3 INCHES.
- 3) MAXIMUM LIFT THICKNESS PRIOR TO COMPACTION
- 4) WATER CONTENT AT TIME OF COMPACTION
- 5) FOR TYPICAL COMPACTION CURVES SEE SHEET 11
- 6) WET MATERIAL THOROUGHLY BUT NOT EXCESSIVELY TO CAUSE SOIL TO ADHERE TO WHEELS OR TRACKS OF EQUIPMENT OR TO BLOW DOWN EQUIPMENT

CONSTRUCTION DETAILS

- 1) THE FOUNDATION SURFACE THROUGH THE BASE AREA OF THE DAM SHL. BE SCARIFIED TO A DEPTH OF 6 INCHES AND CONTACTED PRIOR TO PLACEMENT OF FILL MATERIAL.
- 2) ZONE BOUNDARIES INDICATED ARE APPROXIMATE. ADJUSTMENTS WILL BE MADE BY THE ENGINEER TO PERMIT THE CONTRACTOR TO MAINTAIN THE USABLE REQUIRED EXCAVATION WITHIN THE VEAT LINES OF THE EMBANKMENT.
- 3) TOP 3'-4" THICK FILL AND 1' VERT. ON EACH SIDE OF THE SPILLWAY SECTION AT THE END OF SPILLWAY WILL BE COMPACTED WITHIN THE SHOOTS OF THE EARTH FILL TO ENSURE STABILITY.

-STRIPPED GROUND LINE

-STRIPPED GROUND LINE

N & STA 2:00
RESERVOIR DRAIN
STA 1:50
OF PLUNGE

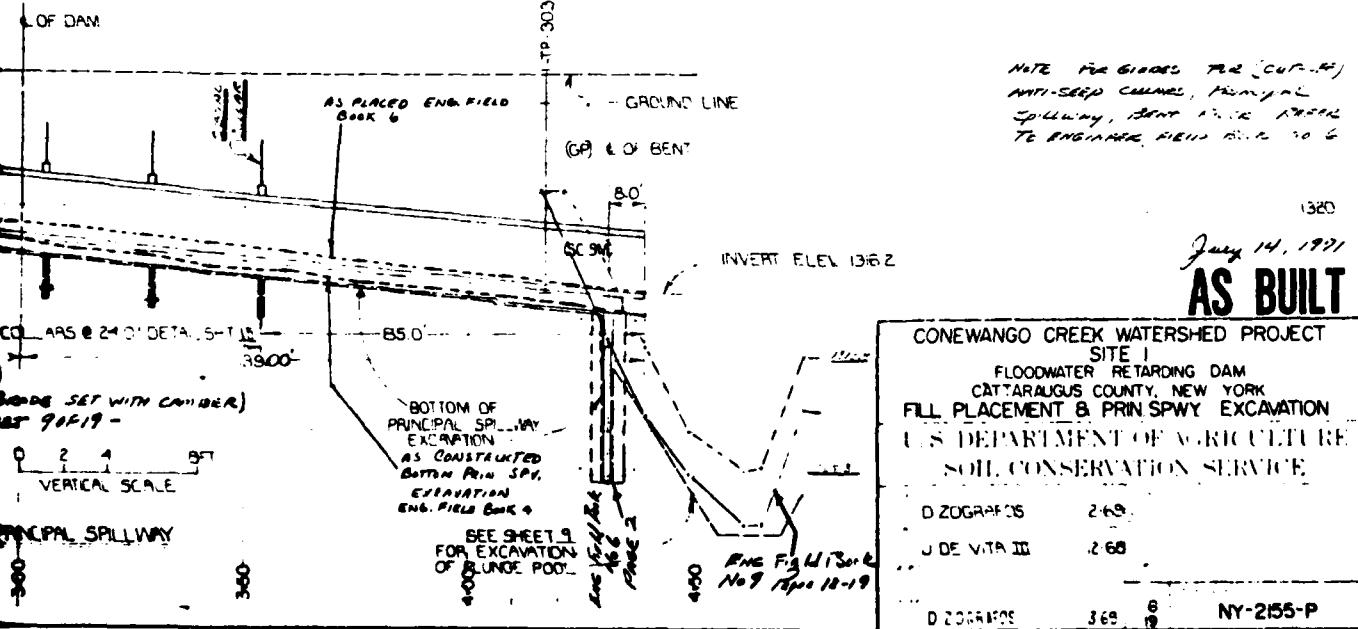


PRINCIPAL SPILLWAY EXCAVATION
SECTION @ ANTI-SEEP COLLARS

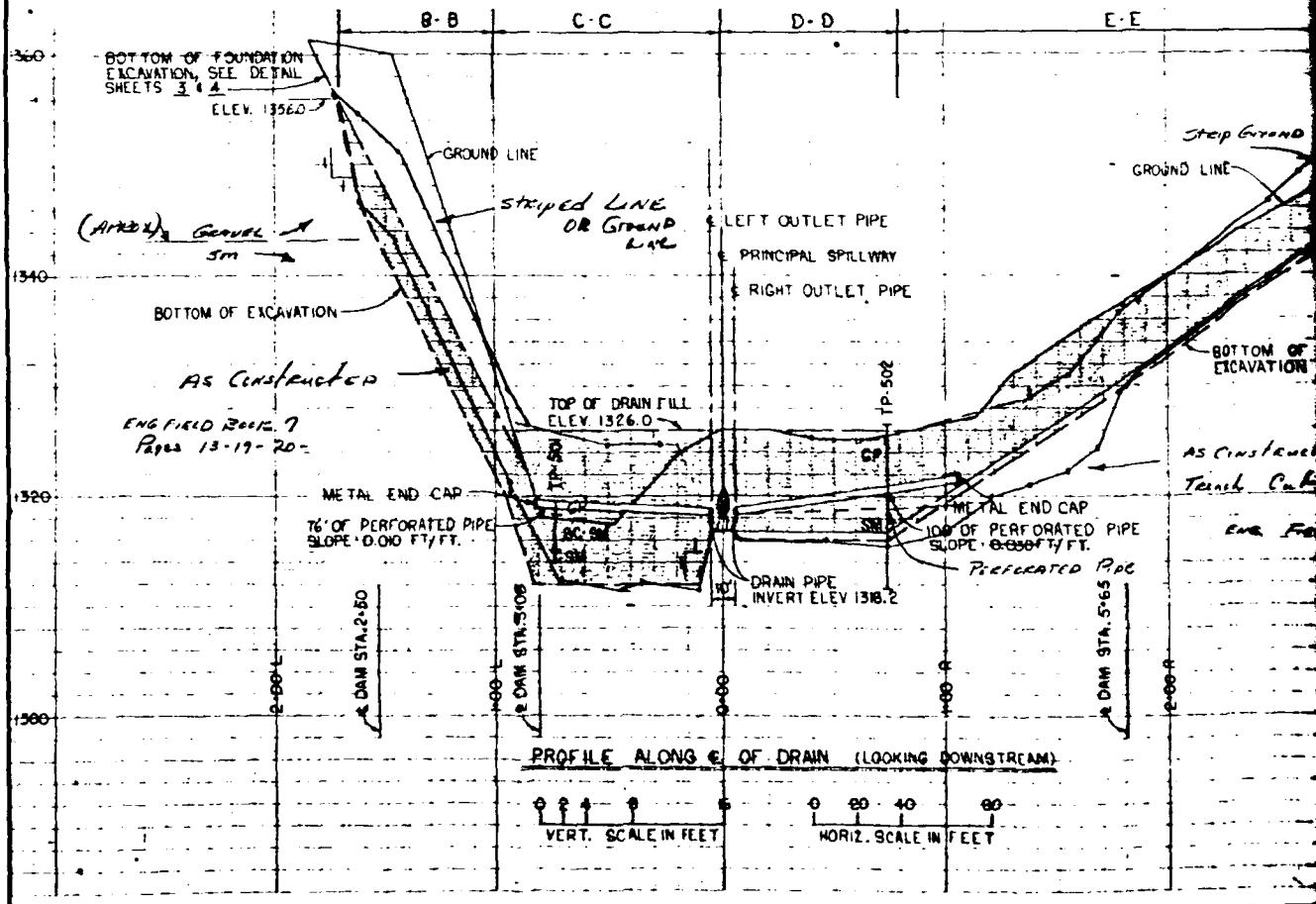
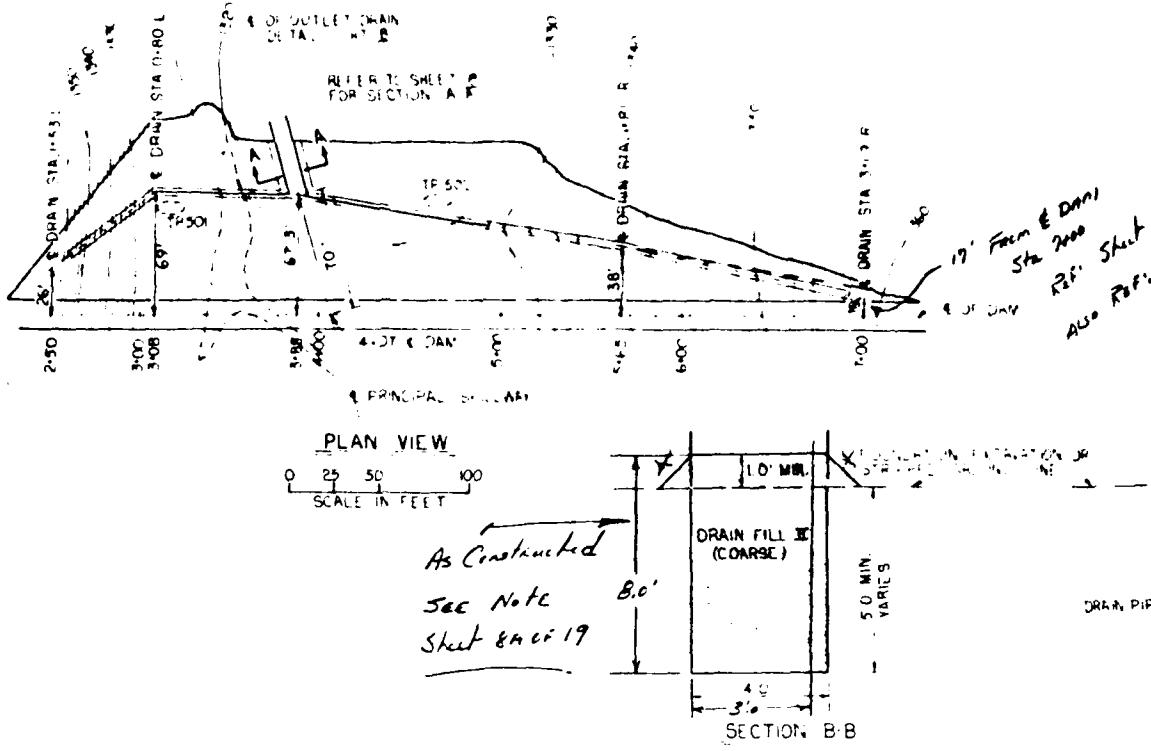
PRINCIPAL SPILLWAY EXCAVATION
SECTION @ STATION 2:10
TYPICAL FROM STATION 1:00 TO STATION 2:00

1330

OF DAM



B-7



GRAIN SIZE DESCRIPTION FOR DRAIN FILL

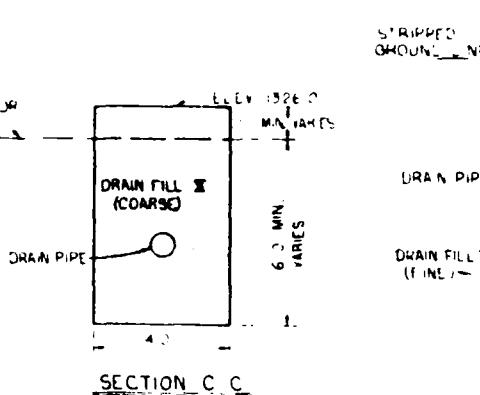
1. DRAIN FILL I (FINE) SHALL MEET THE GRADATION OF ASTM C33-47 FOR FINE AGGREGATE. IN ADDITION, THE PERCENTAGE OF MATERIAL IN DRAIN FILL I FINER THAN A #200 STEEVE SHALL NOT BE MORE THAN 3 PERCENT.
 2. DRAIN FILL II (COARSE) SHALL MEET THE GRADATION OF ASTM C33-47, GRADE A OR CAMP B1. IN ADDITION, THE PERCENTAGE OF MATERIAL IN DRAIN FILL II FINER THAN A #20 STEEVE SHALL NOT BE MORE THAN 10 PERCENT.

BRASIL 1990-1991

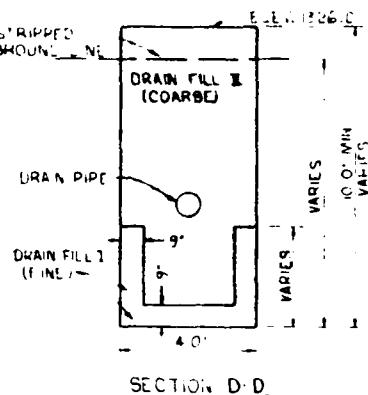
- 1. ALL DRAIN PIPE SHALL CONFORM TO THE SPECIFICATIONS AS SHOWN IN THE DRAWINGS. SIZE OF DRAINS IS TO BE 4"**
 - 2. THE PROFILED AT THE ROOF LEVEL ARE TO BE AS SHOWN AND ONLY APPROVED BY THE ENGINEER. THESE WILL BE ESTABLISHED IN THE FIELD AND NOT ON CONSTRUCTION BY THE CONTRACTOR.**

FACULTY OF ARTS

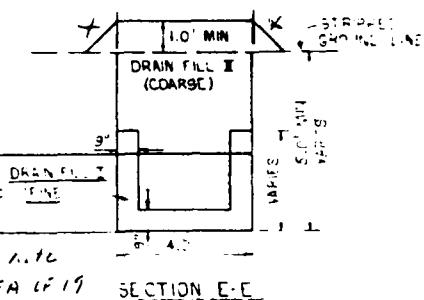
- 670 CU. YDS. DRAIN FILL II (MARKED)
 70 CU. YDS. DRAIN FILL I (UNMARKED)
 264 FT. OF PT. DIA. PERFORATED PIPE
 48 FT. OF PT. DIA. NON-PERFORATED PIPE
 (1) 3-PIECE 3" ELBOW, 90° DIA. (INTERNAL ANGLE)
 (1) 3-PIECE 11½" 3" ELBOW, 90° DIA. (INTERNAL ANGLE)
 (2) SMALL ANIMAL GUARDS
 (2) METAL END CAPS



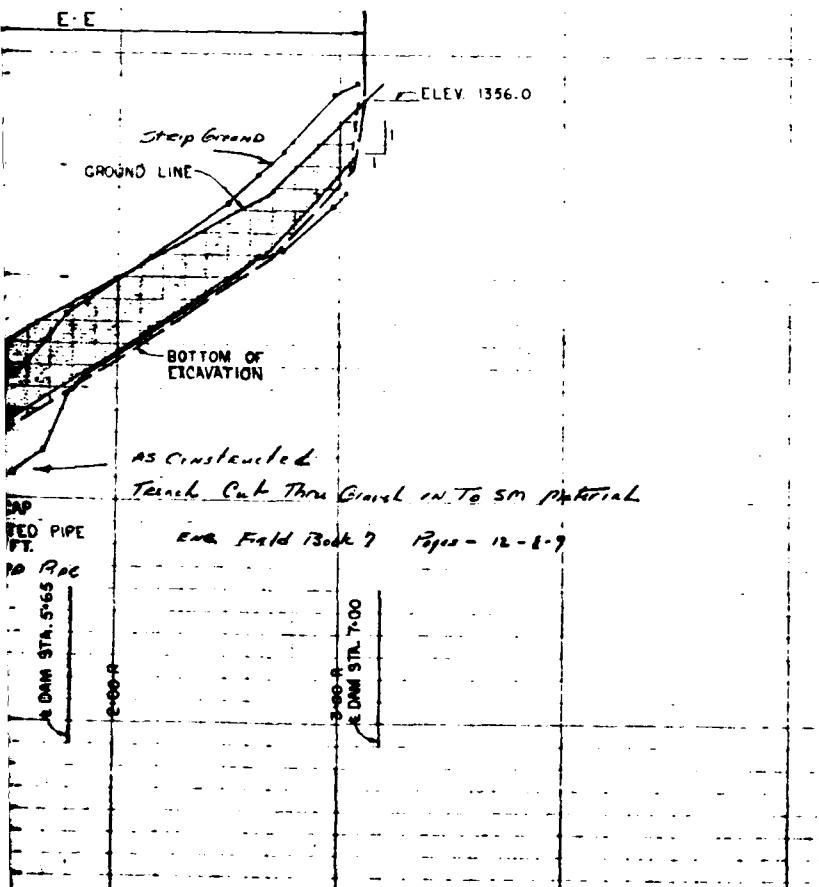
SECTION C.C.



SECTION D-D



7-18A CR 19 SECTION E-E

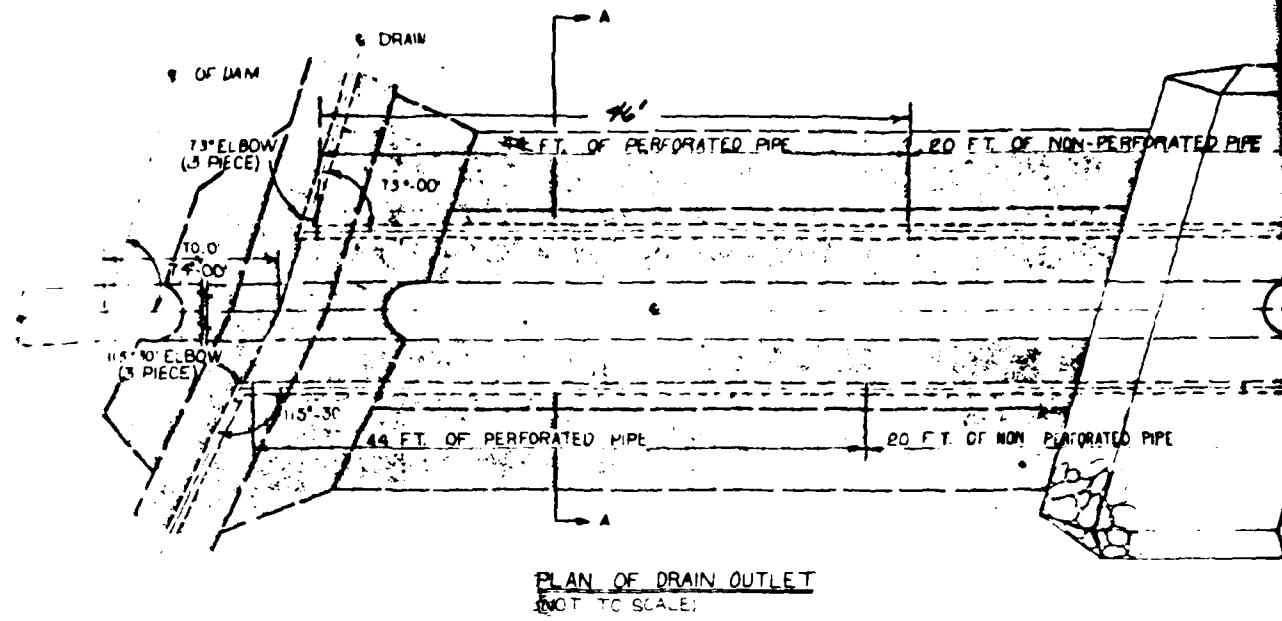


CONTRACT MODIFICATION NO. 3

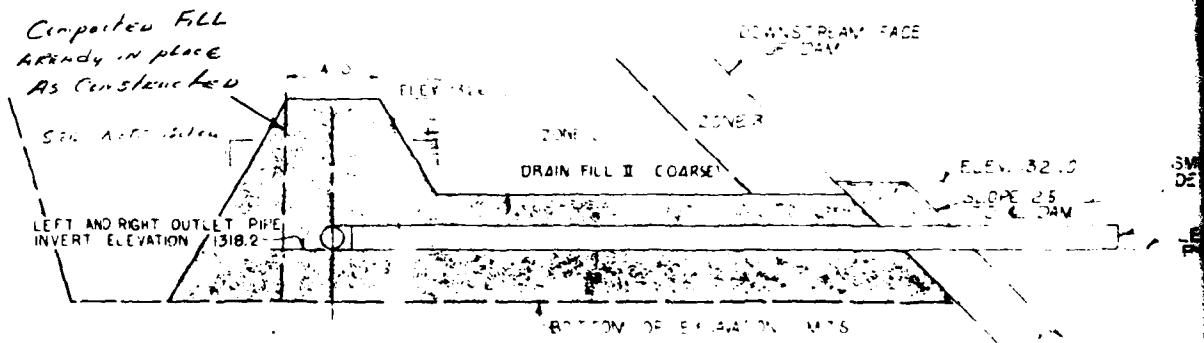
CONEWANGO CREEK WATERSHED PROJECT
SITE I
FLOODWATER RETARDING DAM
CATTARAUGUS COUNTY, NEW YORK
DRAINAGE SYSTEM

**U. S. DEPARTMENT OF AGRICULTURE
SOIL CONSERVATION SERVICE**

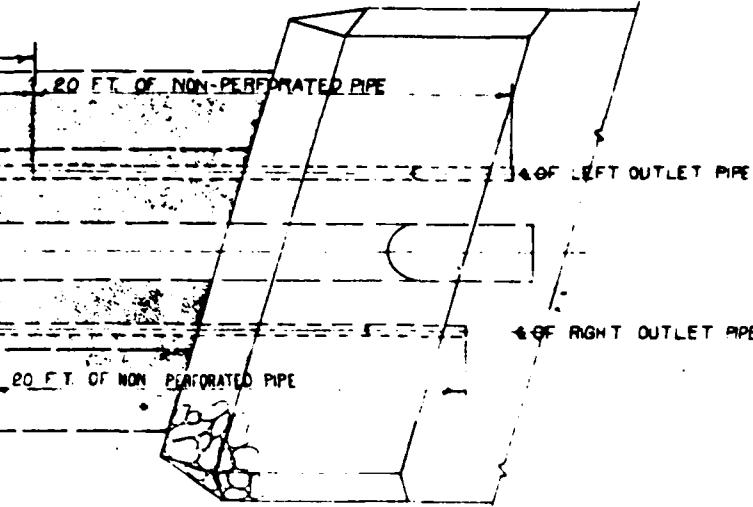
Owner or Drown	A FEHER DENE ZOGRAFOS	4-71 Date 2-69	Address or P.O. 111- 111- 111-
Traced			
Released			
J. E. POLULECH	4-71	Sheet 7A 19	Tracking No. NY-2155-P



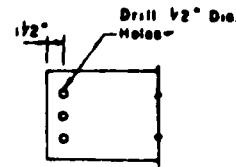
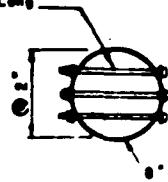
PLAN OF DRAIN OUTLET
(NOT TO SCALE)



PROFILES ALONG DRAIN OUTLETS

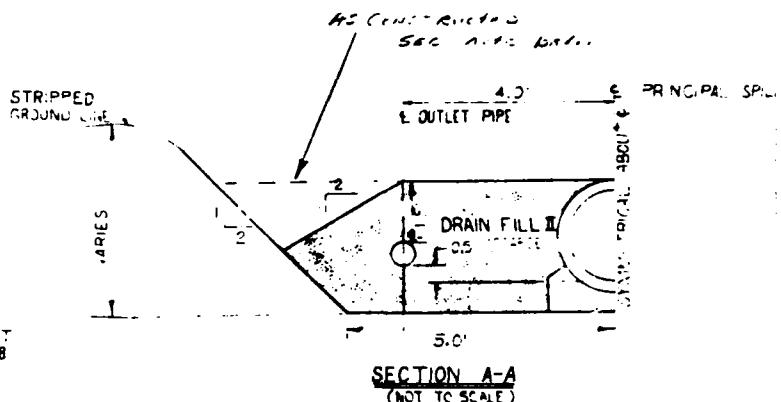
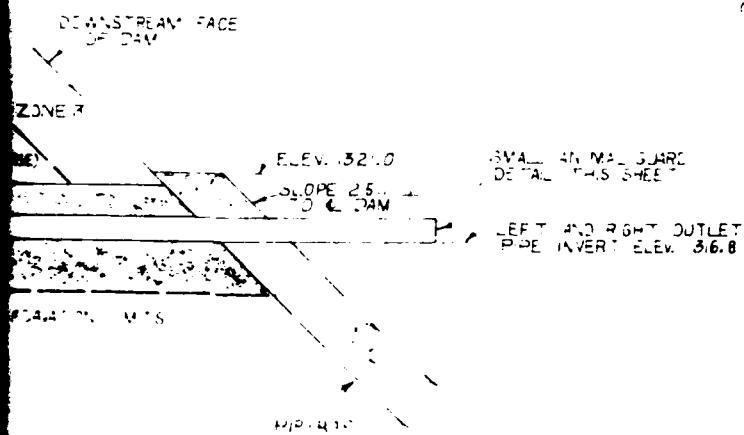


1/2" Dia. Bolts
w/ Hex Nuts And Washers
9" Long



SMALL ANIMAL GUARD DETAILS

0' 6' 12'
Scale

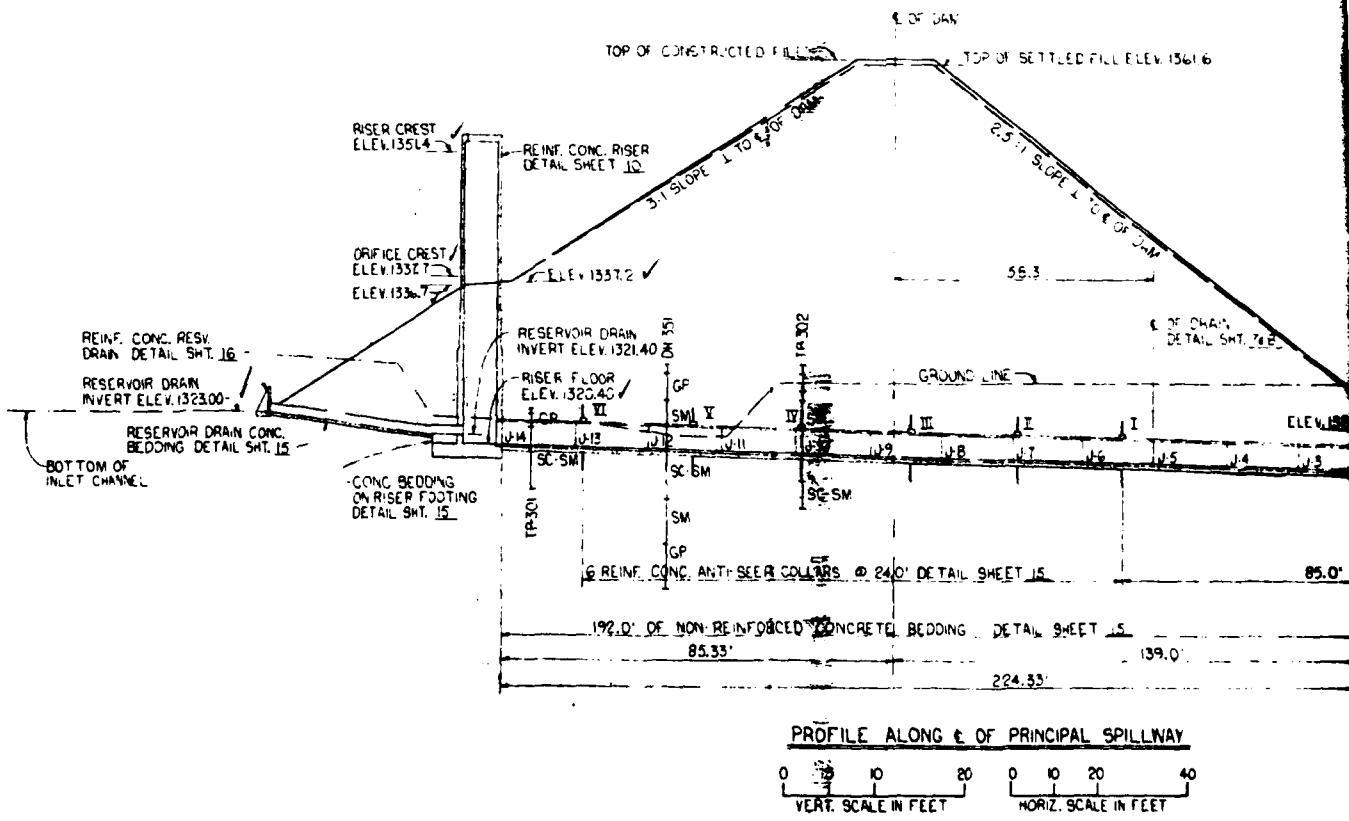
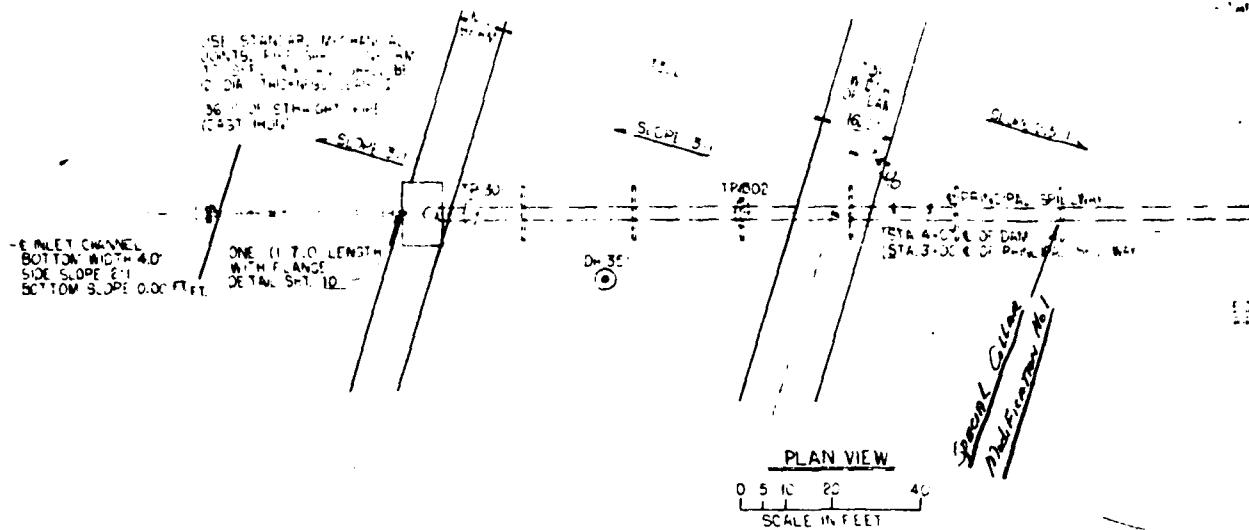


Note (Sheet 7Acr19 - Sheet 5Acr19)
REF: To Job Diary Report No
(107-118)

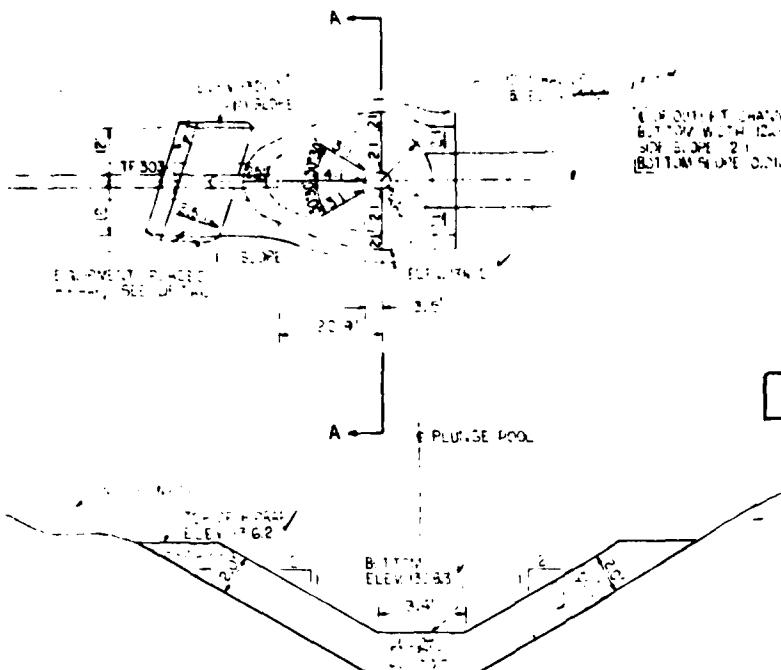
All Changes Made OK by
WESI Links And Dr. Shunklin

CONTRACT MODIFICATION # 3	
CONEWANGO CREEK WATERSHED PROJ.	
SITE 1	
FLOODWATER RETARDING DAM	
CATTARAUGUS COUNTY, NEW YORK	
DRAINAGE SYSTEM	
U. S. DEPARTMENT OF AGRICULTURE	
SOIL CONSERVATION SERVICE	
A. FENNER	4-71
DENE ZOGRAFOS	2/60
B. BURDICK	3/60
JEP D.C.Z. 4-71 NY 388 SA NY-2155-P	

B-9



For room E.O.A. back No 6
2nd floor. made 2-3-4
short traps. made 6-7

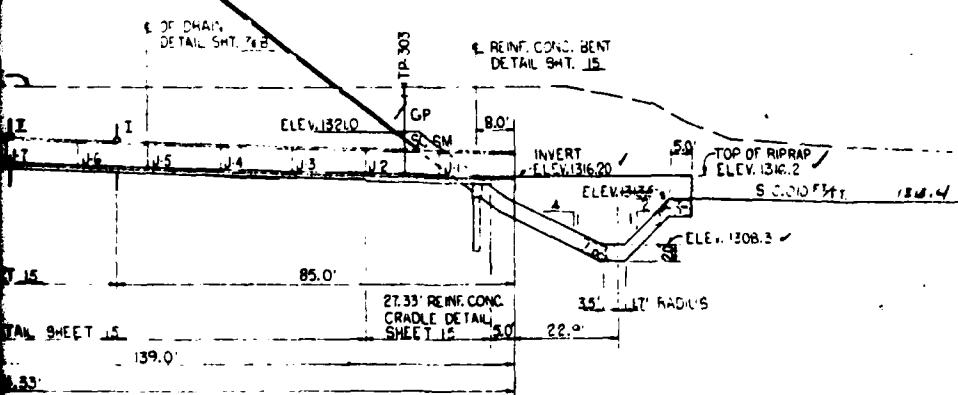


~~SETTLED FILL ELEV. 1361.6~~

SECTION A-A

RIPRAP DETAILS

ALL RIPKAP SHALL BE GRADED FROM A MAX. SIZE OF 18" TO A MIN. SIZE OF 3". A MAX. OF 20% SHALL BE LESS THAN 6" (≈ 10 LB.) IN. A MAXIMUM OF 60% SHALL BE LESS THAN 12" (≈ 80 LB.).



PRINCIPAL SPILLWAY

10 20 40
HORZ. SCALE IN FEET

30 REINFORCED CONCRETE PIPE STRENGTH REQUIREMENTS

RECEIVED
LIBRARY HEAD AT 5 P.M.
MAY 20, 1950 LIBRARY DIRECTOR
WILLIAM H. BROWN
MAY 20, 1950 LIBRARY DIRECTOR
WILLIAM H. BROWN
MAY 20, 1950 LIBRARY DIRECTOR
WILLIAM H. BROWN
MAY 20, 1950 LIBRARY DIRECTOR
WILLIAM H. BROWN

FABRICATION INSTRUCTIONS

(14) .. SECTIONS	(1) 10' SEC. 14 NO. 1 5'-9" RING WALL FITTING FOR 15' WALL
PIPE SUPPLIERS NOTE:	OR PIPE SUPPLIERS NOTE CAST OUTSIDE OF 5'-9" RING AT THE CONCRETE JH ONE SIDE SECTION.

WHEN PIPE IS SUPPLIED IN 20.0' LENGTHS, THE ENGINEER
PROVIDE THE CONTRACTOR WITH A REVISION OF THIS
SHEET SHOWING ORDER OF INSTALLATION AND P/P/E IN EACH
ELEMENT.

July 14, 1921

CONÉWANGO CREEK WATERSHED PROJECT

SITE I

FLOODWATER RETARDING DAM

CATARAUGUS COUNTY, NEW YORK
PLAN PROPOSED OF PRINCIPAL RAILWAY

**PLAN PROFILE OF PRINCIPAL SPILLWAY
U. S. DEPARTMENT OF AGRICULTURE
AGRICULTURAL CONSERVATION SERVICE**

2000-2001

10

2000

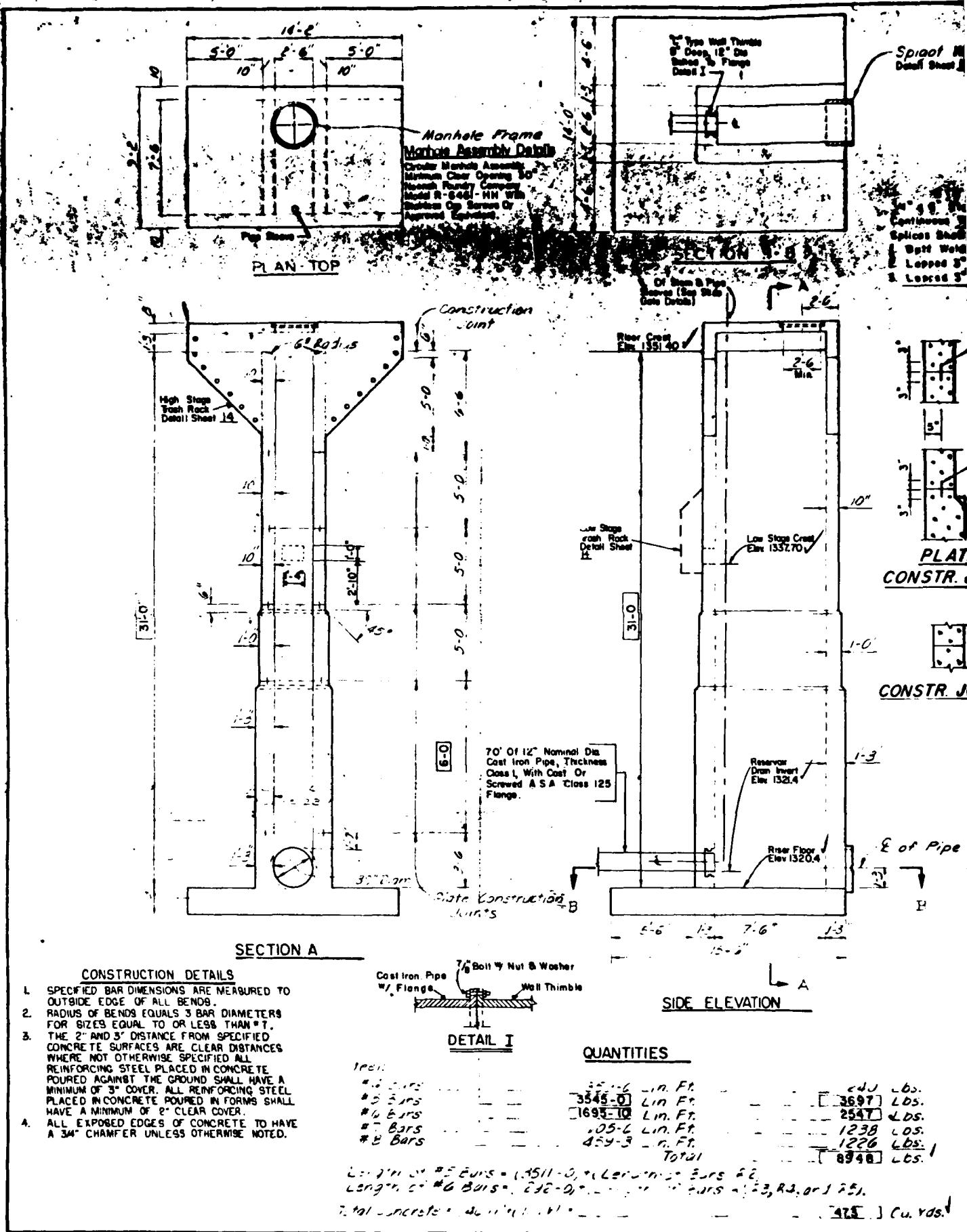
140

M. R.

4

NY-2155-B

B-10



Spout Wall Fitting
Detail Sheet 12

1/8" Steel Plate.
Continuous Threaded Joint.
Splices Shall Be Spliced
Butt Welded
Lapped S" And Bolted
A Lapped S" And Fillet Welded

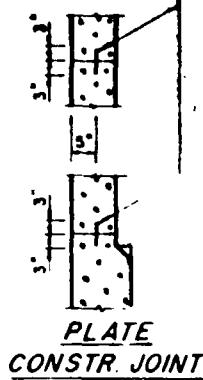
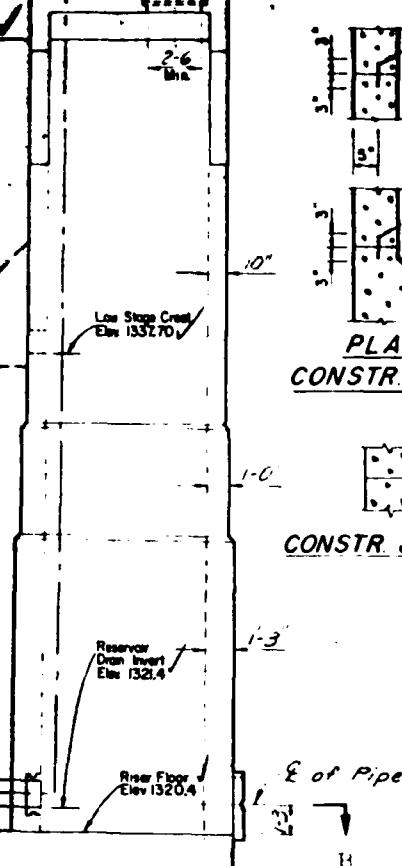


PLATE CONSTR. JOINT



CONSTR. JOINT



12' 7' 6" 13'

12' 5"

A ELEVATION

60.	Lbs.
3697	Lbs.
2547	Lbs.
1238	Lbs.
1226	Lbs.
8940	Lbs.

845 22
845 1/3, R3, or 1/5.

975 Cu. Yds.

STEEL SCHEDULE

Mark	Size	Quant.	Pipe	Length	Type	B	C	Total Length	Mark	Size	Quant.	Pipe	Length	Type	B	C	Total Length
B1	1/2	16	13-6	-	-			216-0									
B2	1/2	14	13-3	-	-			210-0									
B3	1/2	13	7-9	-	-			100-9									
B4	1/2	30	10-3	21	3-5	6-10	303-6										
B5	1/2	16	15-0	-	-			210-0									
B6	1/2	10	13-6	-	-			135-0									
B7	1/2	11	13-6	-	-			140-6									
B8	1/2	8	6-0	-	-			72-0									
B9	1/2	6	7-9	21	1-0	6-9	147-3										
B10	1/2	19	7-9	21	1-0	6-9	147-3										
B11	1/2	24	8-6	-	-			112-0									
B12	1/2	3	3-6	-	-			17-6									
B13	1/2	3	2-9	-	-			8-3									
B14	1/2	2	2-9	-	-			8-6									
B15	1/2	10	6-9	21	0-10	3-11	67-6										
B16	1/2	18	9-3	21	3-4	5-11	166-6										
R1		12	7-7	-	-			166-10									
R2		4	8-6	-	-			34-0									
R3		2	-	-	-			7-0									
R4		2	5-5	-	-			151-8									
R5		8	2-3	21	3-4	5-11	74-0										
R6		4	8-6	-	-			119-0									
R7		1	3-6	-	-			35-0									
R8		1	2-8	-	-			95-4									
R9		3	8-3	21	3-1	5-7	315-0										
R10		4	8-3	21	2-0	5-4	110-0										
R11		22	6-9	-	-			13-0									
R12		14	8-3	-	-			7-18									
R13		1	3-6	-	-			32-0									
R14		30	3-6	-	-			7-10									
R15		10	2-3	-	-			7-0									
R16		30	4-3	-	-			27-0									
R17		3	3-0	21	1-0	9-3	33-3										
R18		13	11-4	-	-			120-0									
R19		14	4-3	-	-			113-0									
R20		5	3-3	-	-			20-0									
R21		21	3	-	-			-									
R22		30	5-1	-	-			29-3									
R23		13	6-1	-	-			18-0									
R24		5	2-2	-	-			18-0									
R25		14	8-0	21	1-0	5-3	220-0										

Bases Checked - Framed To meet Specs - bases here Republic Steel Corporation 10-10-70
Date 28-1970

John Galloway
C. Big Test

TYPE I

TYPE II

BLOCKED IN DIMENSIONS
NOT TO SCALE

AS BUILT

CONE WANGO CREEK WATERSHED PROJECT

SITE 1

FLOODWATER RETARDING DAM
CATARAUGUS COUNTY, NEW YORK

RISER STRUCTURAL DETAILS

U.S. DEPARTMENT OF AGRICULTURE
SOIL CONSERVATION SERVICE

ROBERT D. ZOGRAFOS

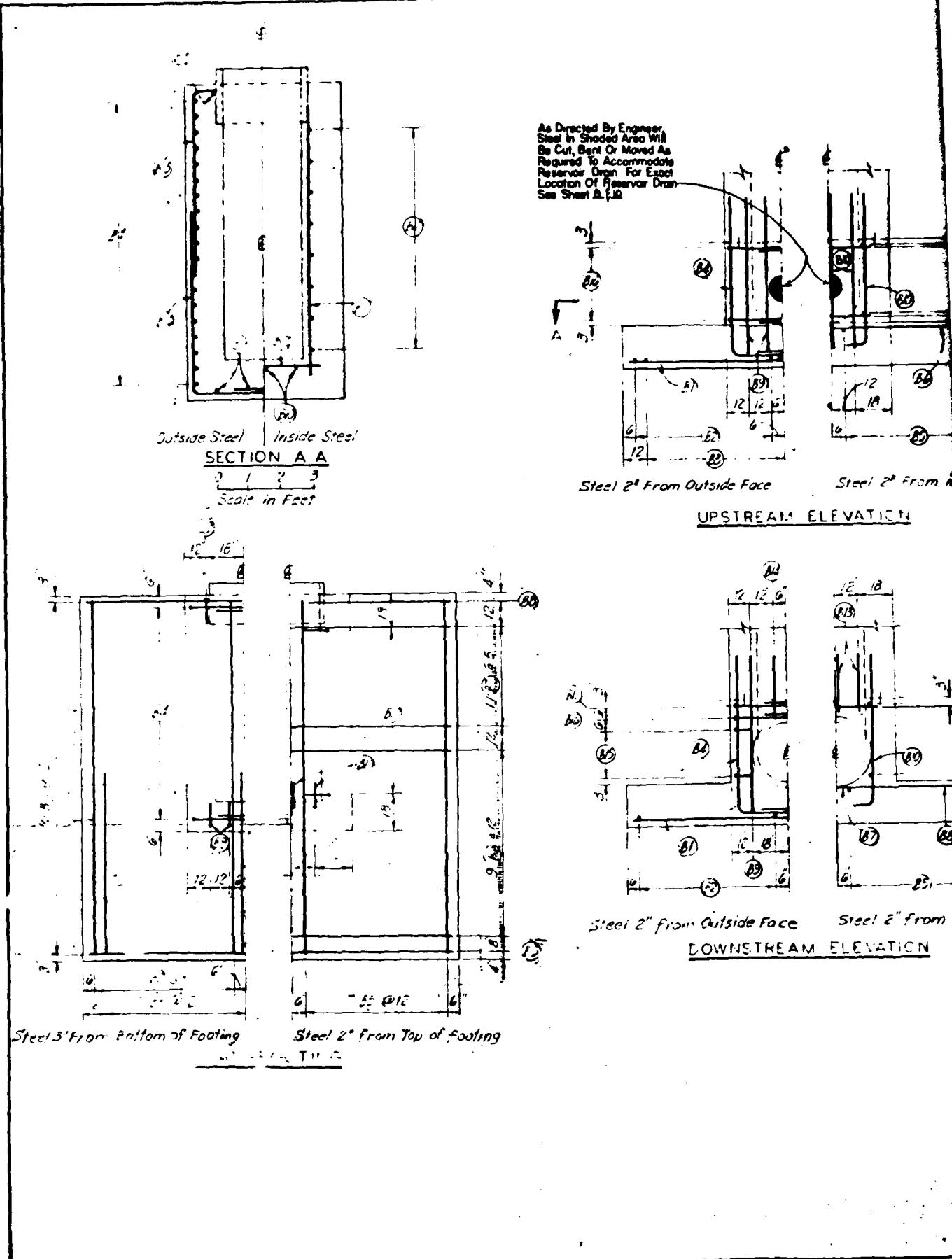
12/00

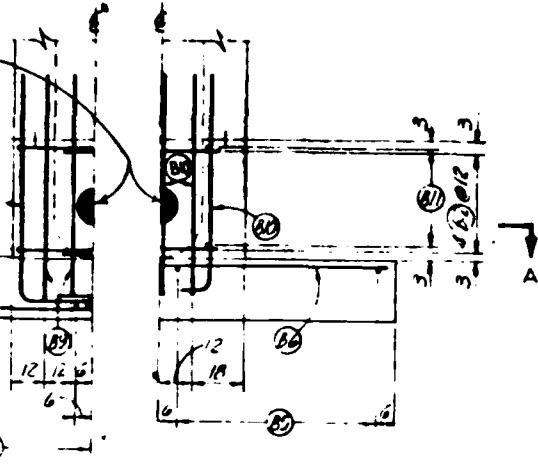
J. E. POLULECH 4/80 10 NY-2155-P

B-11

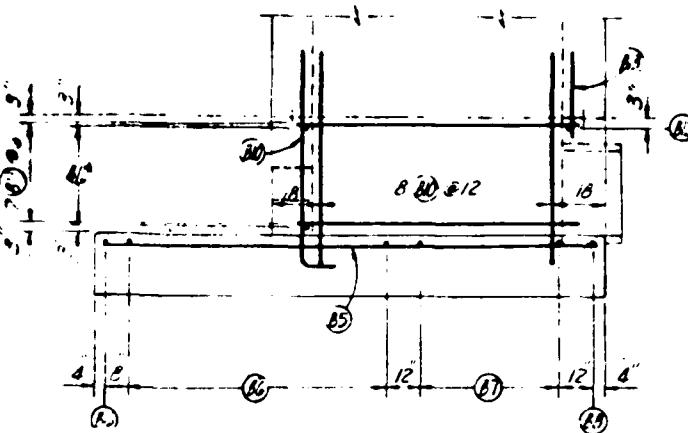
SLIDE GATE DETAILS

- 1 12" dia flat frame slide gate (self contained unit)
- 2 class 0.32
- 3 slide gate shall conform to Spec. 801 and shall be type MHS 1
- 4 "C" type wall thimble 8" deep
- 5 pipe sleeve, stem & stem guides sized and spaced according to manufacturer's recommendations. removable t handle wrench, wrench socket and top of stem located within pipe sleeve.
- 6 paint in accordance with Spec. 22
- 7 holes drilled in back flange of wall thimble by gate manufacturer according to A.S.A. class 125 flange spec.
- DIAMETER OF BOLT CIRCLE 17"
- NUMBER OF BOLT HOLES - 12"
- DIAMETER OF BOLT HOLES - 1"

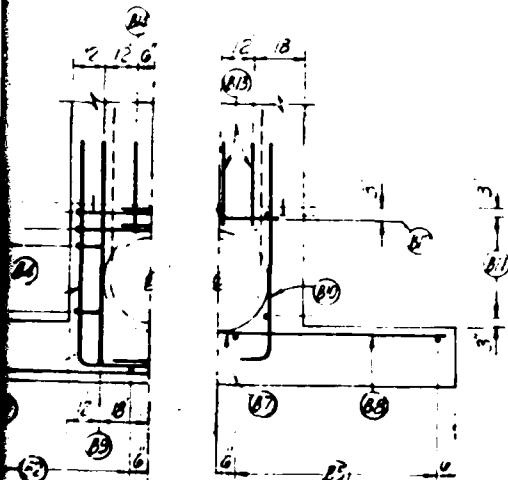




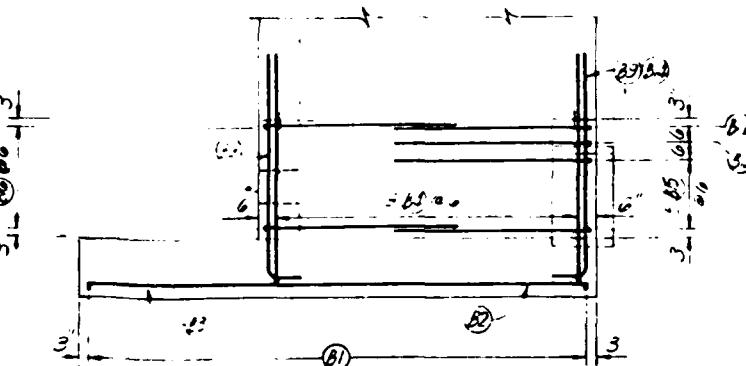
Outside Face Steel 2" From inside Face
UPSTREAM ELEVATION



Steel: 2" From Inside Face
and 2" From Top of Footing
SIDEWALL ELEVATION



Outside Face Steel 2" from Inside Face
OWNSTREAM ELEVATION



See J^o From Outside Face and
J^o From Bottom of Footing

July 14, 1971

AS BUILT

AS Scale in Feet
unless Otherwise Shown

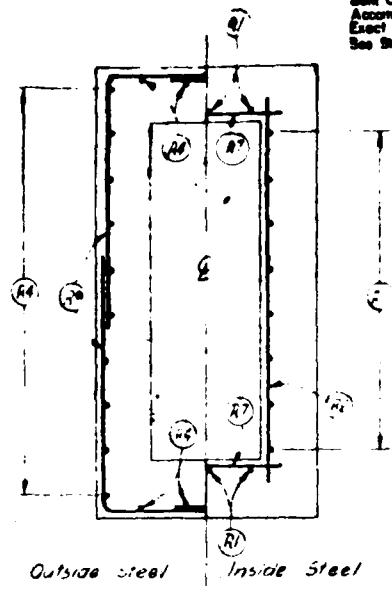
**CONEWANGO CREEK WATERSHED PROJECT
SITE 1**
FLOODWATER RETARDING DAM
CATTARAUGUS COUNTY, NEW YORK
RISER STRUCTURAL DETAILS

U. S. DEPARTMENT OF AGRICULTURE
SOIL CONSERVATION SERVICE

Adopted	Date	Approved by
ZOGRAFOS	1-69	1-1969
Drawn		
Traced		
Checked		
		Drawing No. 100
		Rev II Date 1-1969
		NY-215-P

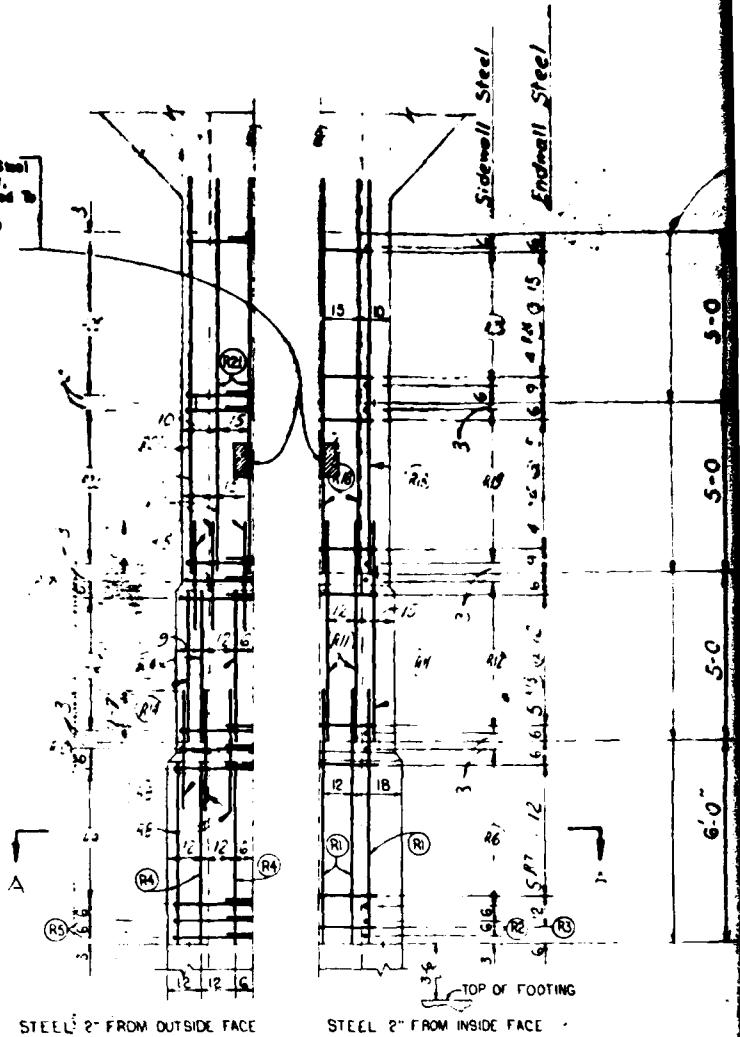
B-12

As Directed By Engineer, Steel
In Shaded Area Will Be Cut.
Bent Or Moved As Required To
Accommodate Orifice Per
Exact Location Of Orifice
See Street 9610



Outside Steel | Inside Steel

SECTION A-A



ENDWALL ELEVATION

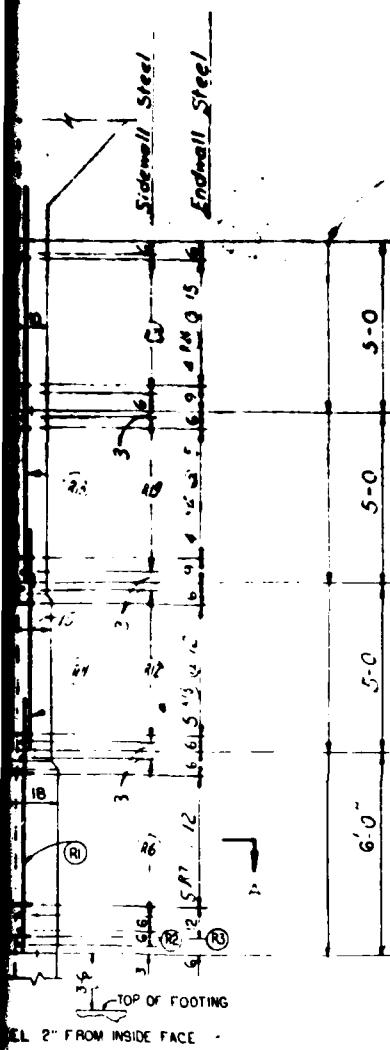
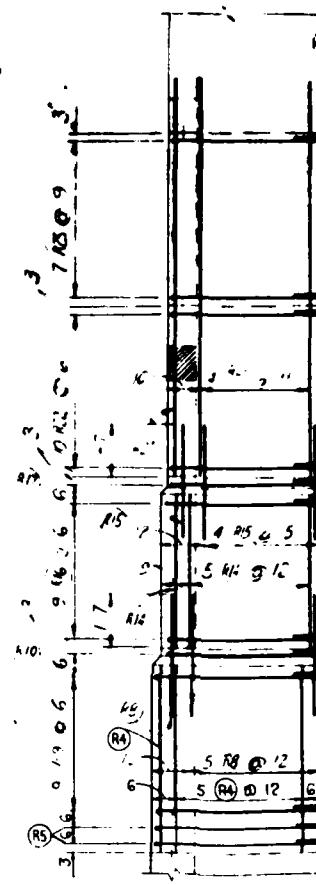
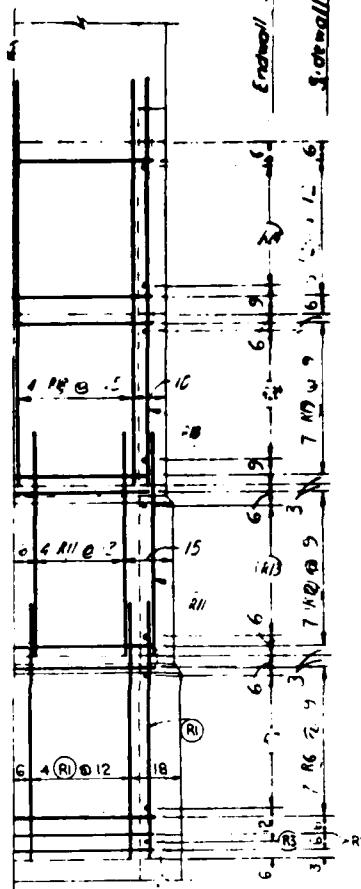


Plate Construction
Joints



STEEL 2' FROM OUTSIDE FACE



STEEL 2' FROM INSIDE FACE

SIDEWALL ELEVATION

July 14, 1971
Scale in Feet
AS BUILT
Unless Otherwise Shown

CONEWANGO CREEK WATERSHED PROJECT
SITE I

FLOODWATER RETARDING DAM
CATTARAUGUS COUNTY, NEW YORK

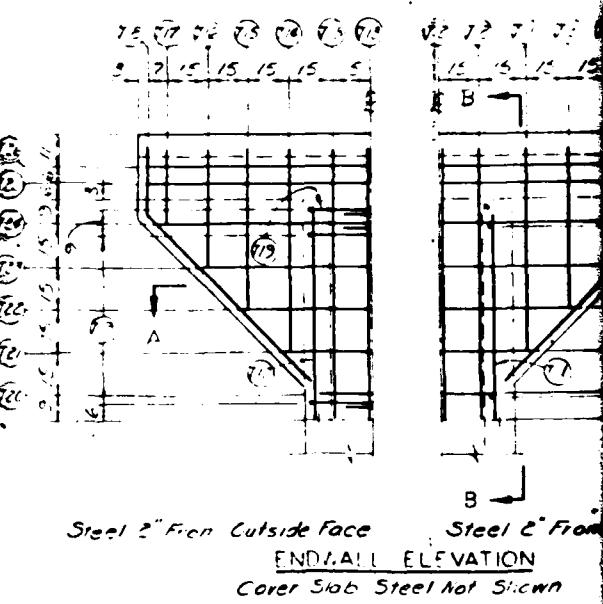
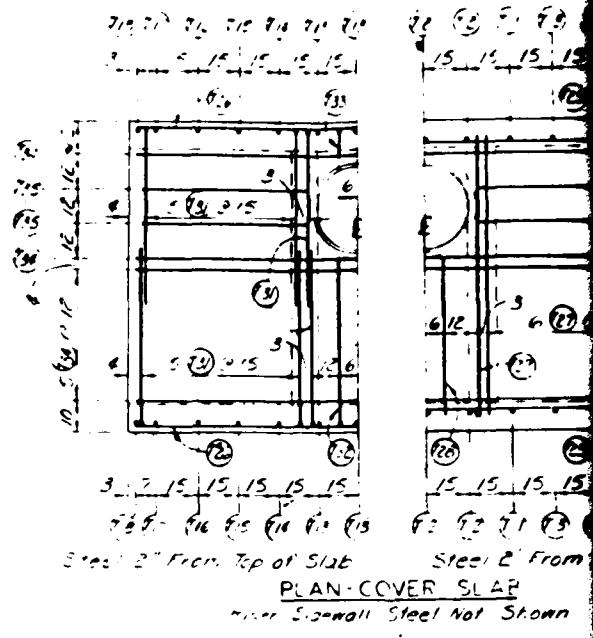
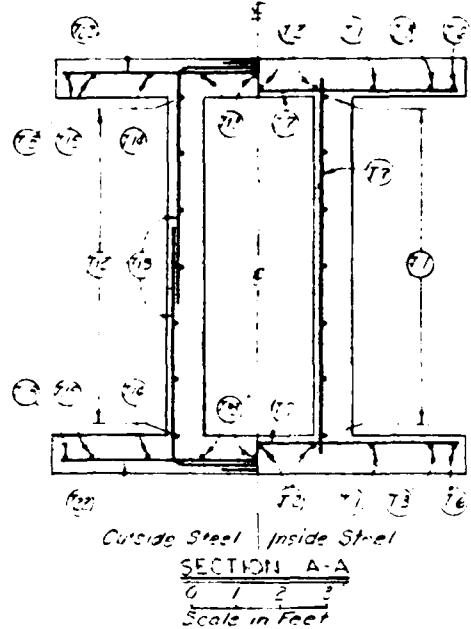
RISER STRUCTURAL DETAILS

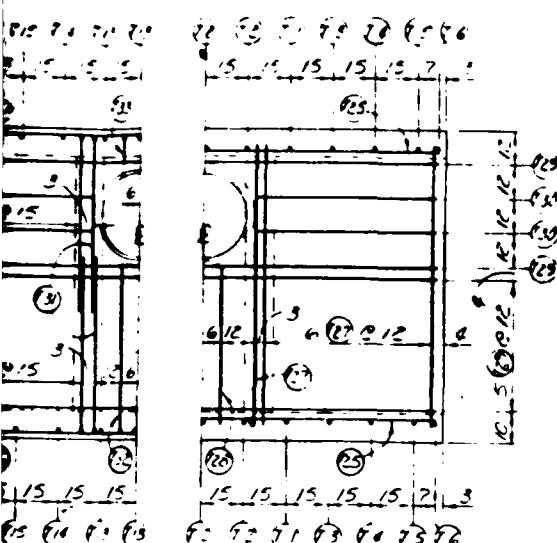
U. S. DEPARTMENT OF AGRICULTURE
SOIL CONSERVATION SERVICE

Adopted New York State

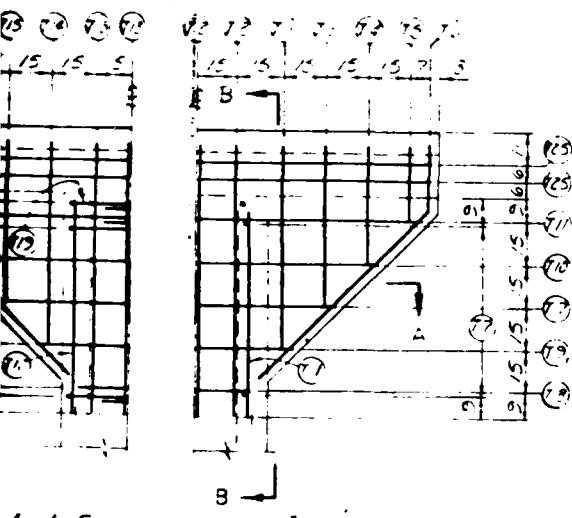
NY-255-P

B-13

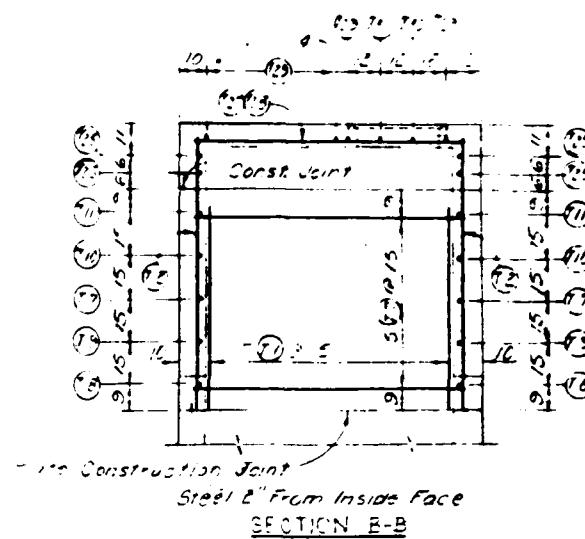




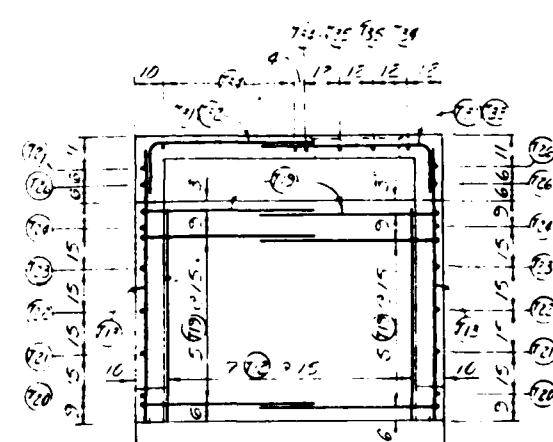
PLAN-COVER SLAB
Minor Steel Not Shown



END-ELEVATION
over Slab Steel Not Shown



SECTION A-A



SECTION B-B

July 14, 1971
0 2 4
Scale in Feet
Unless Otherwise Shown

CONEWANGO CREEK WATERSHED PROJECT

SITE I

FLOODWATER RETARDING DAM
CATTARAUGUS COUNTY, NEW YORK

RISER STRUCTURAL DETAILS

U. S. DEPARTMENT OF AGRICULTURE
SOIL CONSERVATION SERVICE

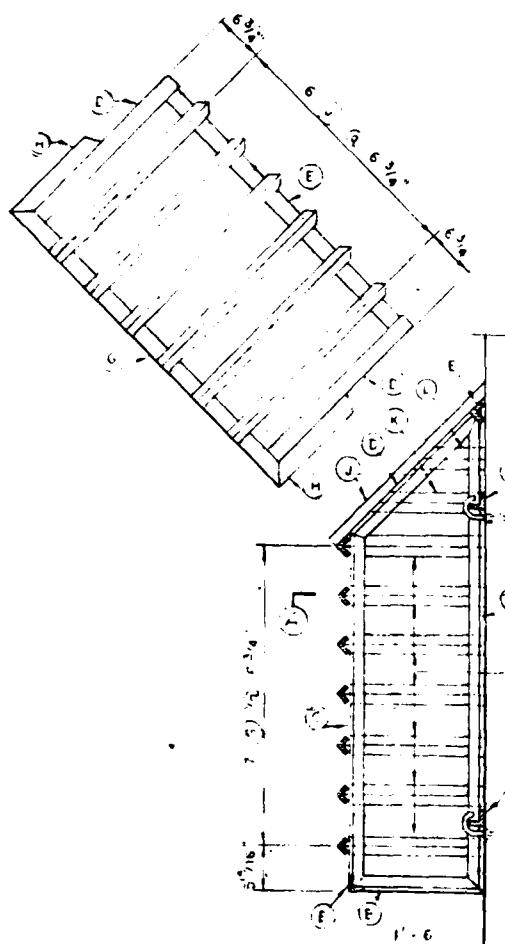
DESIGNER	OZOGAROS	DATE	1-69
APPROVED BY		APPROVED BY	
13	14	15	16
13	14	15	16
NY-2155-P			

B-14

LOW STAGE TRASH RACK BILL OF MATERIALS			
ITEM	SIZE	LENGTH	QUANTITY
Angle A	2" x 2" x 1/4"	9' - 6"	2
Angle B	-	1' - 6"	2
Angle C	-	4' - 0"	2
Angle D	-	2' - 1 1/2"	2
Angle E	-	3' - 7 1/4"	2
Angle F	-	3' - 10 1/2"	2
Angle G	-	4' - 23 1/2"	7
Angle H	-	1' - 7 3/8"	14
Angle J	-	2' - 5 5/8"	6
Angle K	-	1' - 5 1/2"	2
Angle L	-	0' - 6 1/2"	2
"HOOK" Bolts	5/8" Dia.	2"	6
Pipe Sleeves	3/4" Dia	-	4

CONSTRUCTION DETAILS

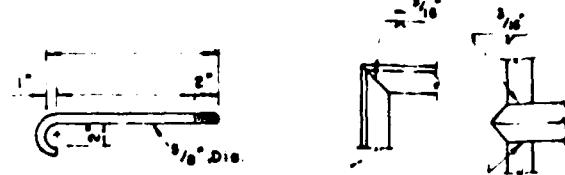
- 1 All points of contact between angles to be welded.
- 2 Low stage trash rack to be galvanized in accordance with Spec II-9. If necessary for galvanizing, trash rack may be fabricated in sections and bolted with the approval of the Engineer.
- 3 Material in low stage trash rack shall conform to Spec II-7 for structural carbon steel plates, shapes and bars.



SECTION ON E

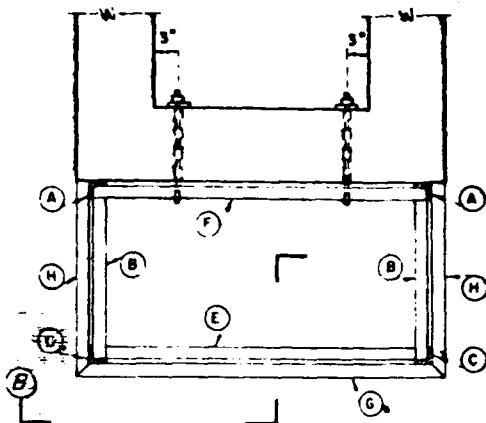
SCALE E

LOW STAGE TRASH RACK DETAILS

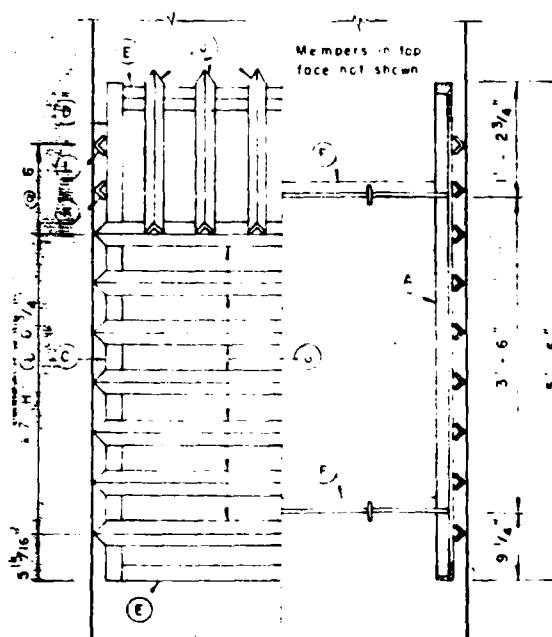


"HOOK" BOLT
Supply with washer and Type 2 nut

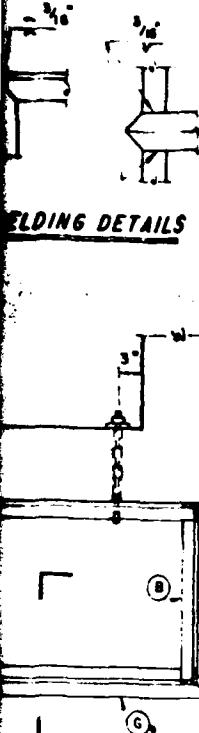
WELDING DETAILS



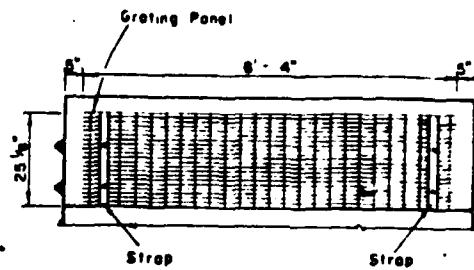
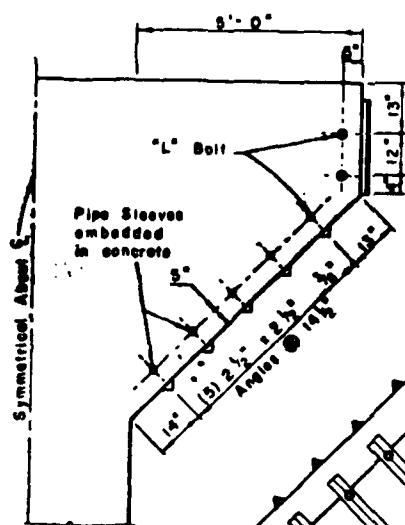
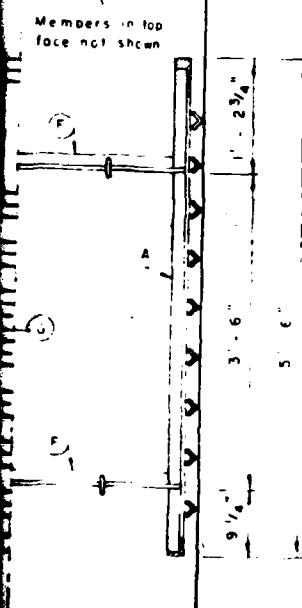
SECTION AA



SECTION BB

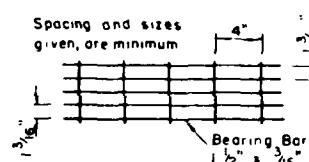
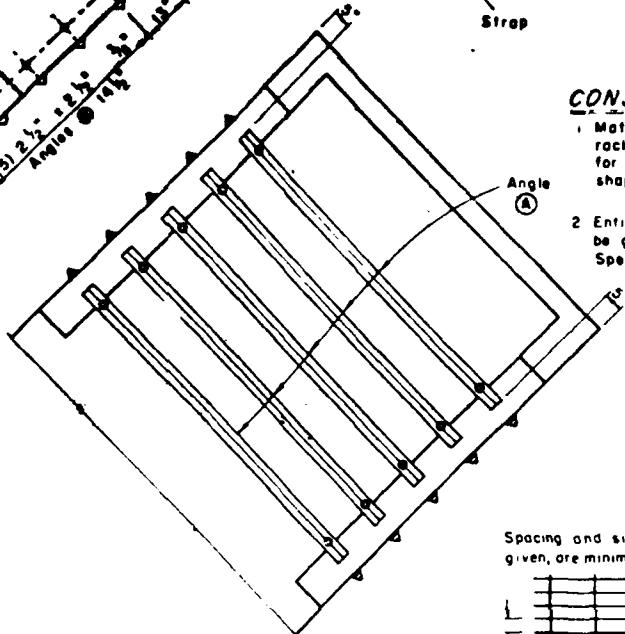


SECTION AA



CONSTRUCTION DETAILS

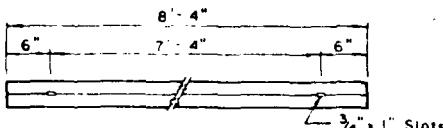
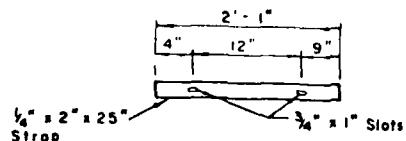
- Material in high stage trash rack shall conform to Spec II7 for structural carbon steel plates, shapes, and bars.
- Entire high stage trash rack to be galvanized in accordance with Spec II9.



GRATING PANEL

"L" BOLT (Galvanized)

Supply with washers and Type 2 nuts.



STRAP

ANGLE A

HIGH STAGE TRASH RACK DETAILS

Scale 1:200

July 14, 1971
AS BUILT

HIGH STAGE TRASH RACK BILL OF MATERIALS			
ITEM	SIZE	LENGTH	QUANTITY
Angles (A)	2 1/2" x 2 1/2" x 3/8"	8' - 4"	10
Strap	1/4" x 2" x 25"	-	4
"L" Bolt	3/8" Dia	8' x 13"	28
Grating Panel	25 1/4" x 8' - 4"	-	2
Sleeves	3/4" Dia	10"	28

CONEWANGO CREEK WATERSHED
SITE I
FLOODWATER RETARDING DAM
CATTARAUGUS COUNTY, NY
RISER TRASH RACKS

U. S. DEPARTMENT OF AGRICULTURE
SOIL CONSERVATION SERVICE

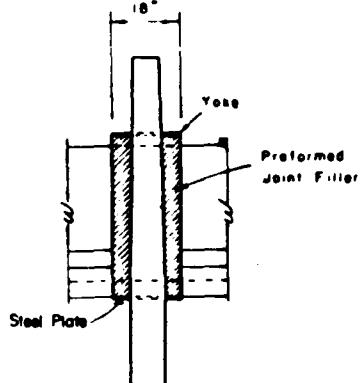
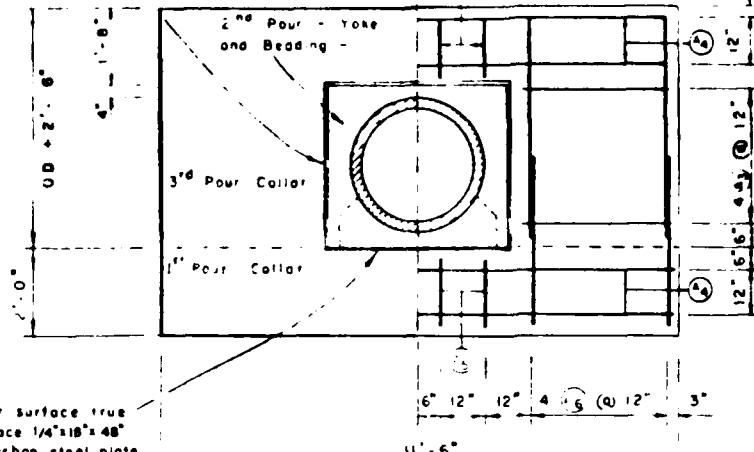
Approved D. ZOGRAFOS	Date 1/69
Supervisor W. H. Morgan	14
Technician R. L. Allen	19
File No. NY-2155-P	

B-15

1 1/2" Preformed Joint Filler
18" Wide, Type 1 - Spec. 56

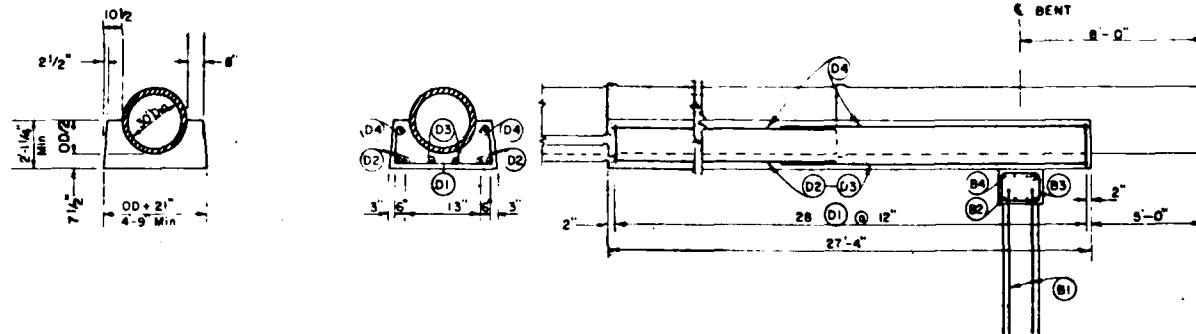
Symmetrical About E

3'-9" 2'-0" 1'-2" 1'-2" 4'-0" 4'-12" 3'



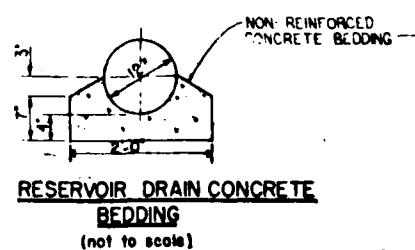
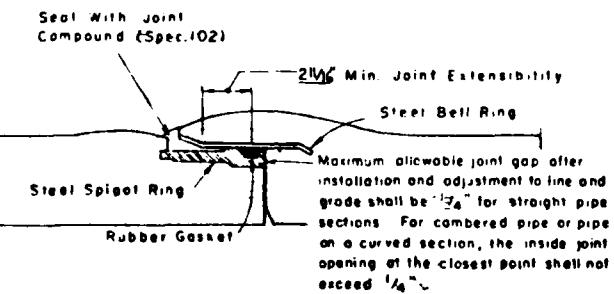
REINFORCED CONCRETE ANTI-SEEP COLLAR

6 - Req'd.

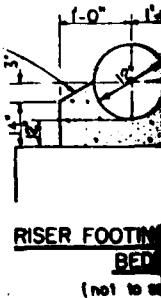


REINFORCED CONCRETE CRADLE AND BENT DETAILS

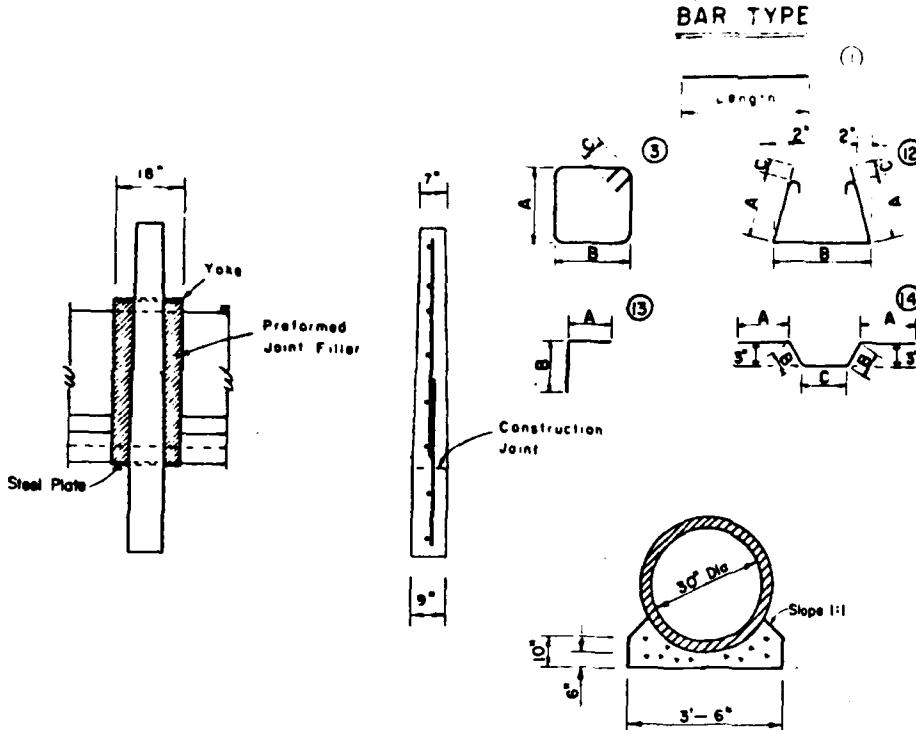
0 2 4 FT.
SCALE



**RESERVOIR DRAIN CONCRETE
BEDDING**
(not to scale)

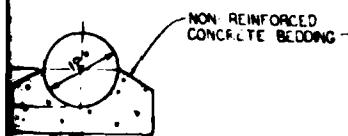
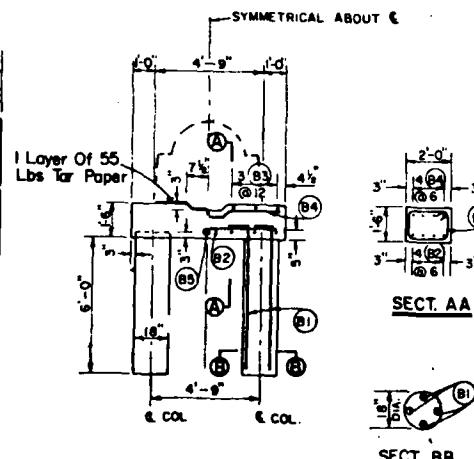
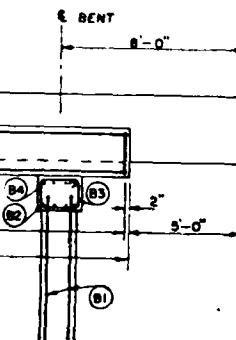


REINFORCED CONCRETE PIPE - JOINT DETAILS

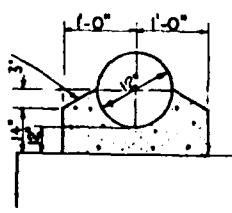


COLLAR

3 - Reg'd.



NOIR DRAIN CONCRETE
BEDDING
(not to scale)



RISER FOOTING CONCRETE
BEDDING
(not to scale)

ANTI-SEEP COLLAR STEEL SCHEDULE						
Mat#	Size	Length	Weight	Length	Weight	Length
A-1	4		4		20	20
A-2	4	5'-0"	5		48	240-0
A-3	4	3'-3"	6		40	240-0
A-4	4	11'-0"	4		24	264-0
A-5	4	1'-6"	4		20	36-0
A-6	4	3'-9"	6		48	180-0

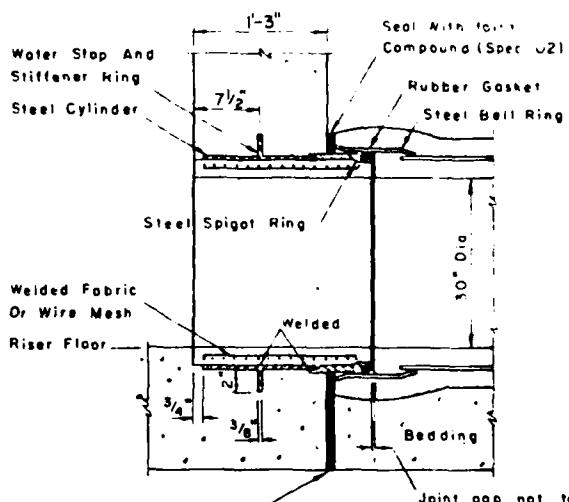
Bass Chalked - young to mat. sizes - Bass from Regal Blue
Steel Corp. Works June 23 1930

STEEL

No	Bar	Fl	729	C. Eng. back.
No 4	<u>1242.2</u>	Ft.	<u>874</u>	Lbs
No 5	<u>82.7</u>	Ft.	<u>86</u>	Lbs PEG
No 7	<u>58.7</u>	Ft.	<u>120</u>	Lbs Contrast MODIFICATION
No 8	<u>25.0</u>	Ft.	<u>67</u>	Lbs No 1
No 9	<u>119.3</u>	Ft.	<u>406</u>	Lbs

CONCRETE 20.2
REINFORCED 22.6 Cu Yds
NON-REINF. 22.8 Cu Yds

CONSTRUCTION DETAILS SHEET 10



1/2" Preformed Joint Filler.
Type I. (Spec. 106) Placed
between riser and bedding.

SPIGOT WALL FITTING?

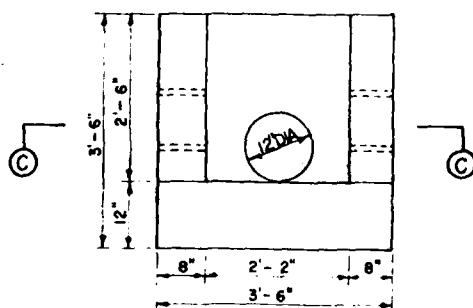
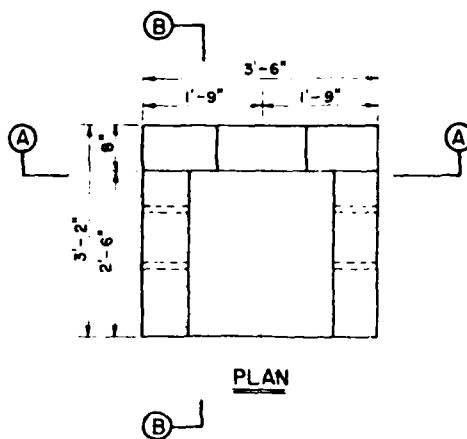
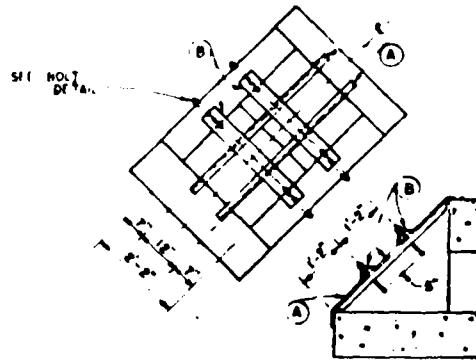
AS BUILT

CONEWANGO CREEK WATERSHED PROJECT

SITE I
FLOODWATER RETARDING DAM
CATTARAUGUS COUNTY, NEW YORK
CONDUIT DETAILS

**U. S. DEPARTMENT OF AGRICULTURE
SOIL CONSERVATION SERVICE**

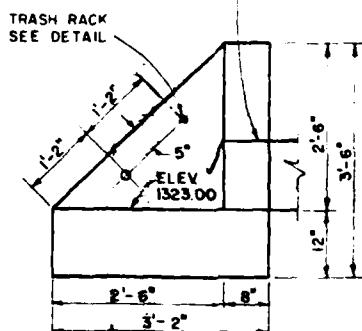
SOIL CONSERVATION SERVICE		Date
Designed	D. ZOGRAFOS	12/68
Brown	M.T. Bremering Co.	No. 68
Traced		
Charged	D.C.E.	5-99
Approved by _____		Date _____
		Time _____
		Time _____
		Initials _____ Drawing No. _____
		No. 15 NY-2155-P



POND DRAIN INLET TRASH RACK DETAILS

NOT TO SCALE

1/2" PREFORMED JOINT FILLER
MAT'L SPEC 106

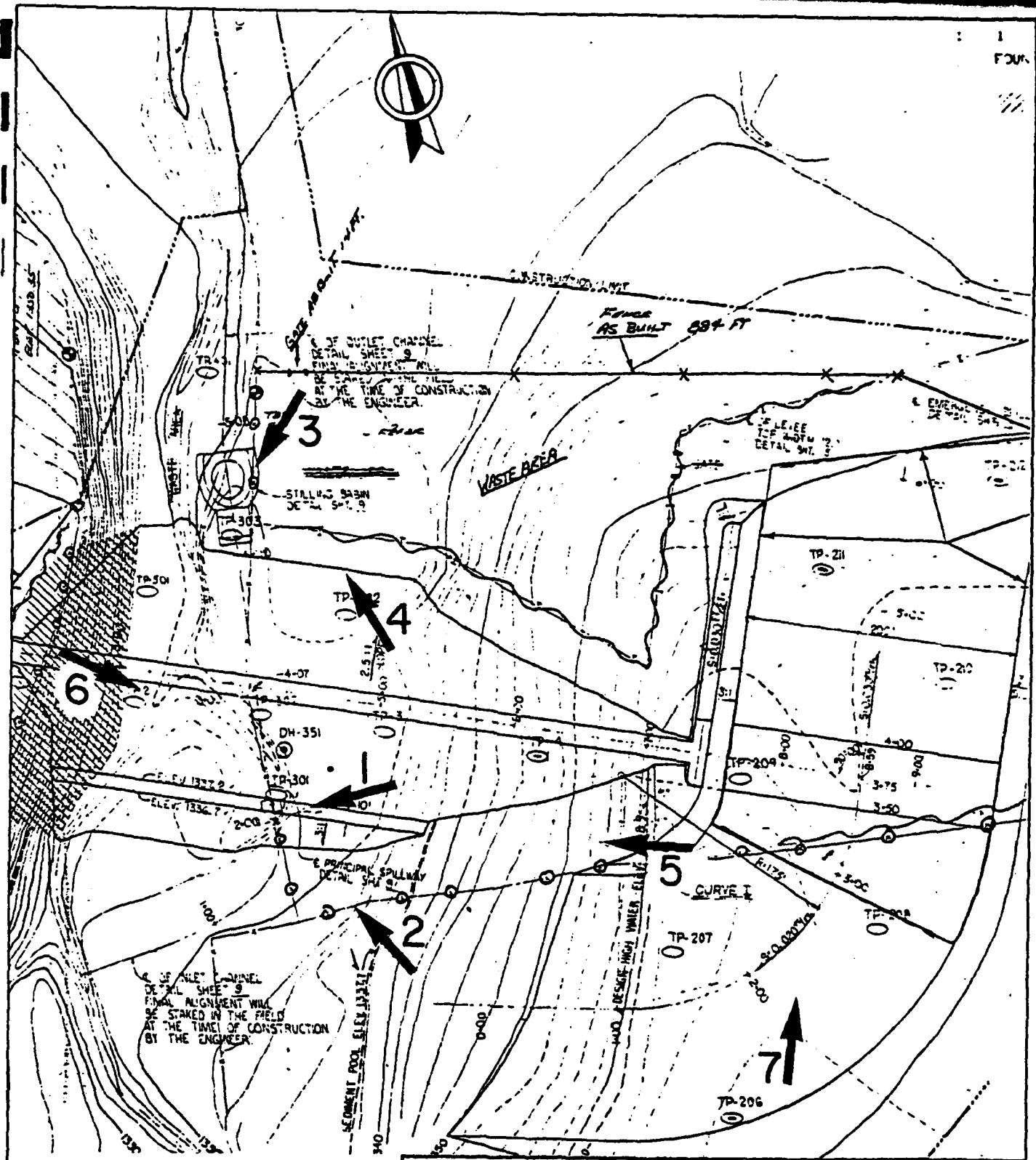


SECTION ALONG C

0 3 6 12 24
SCALE IN INCHES

APPENDIX C

PHOTOGRAPHS



DAVIS BROOK DAM (SITE I)

NY00564

PHOTO ORIENTATION PLAN

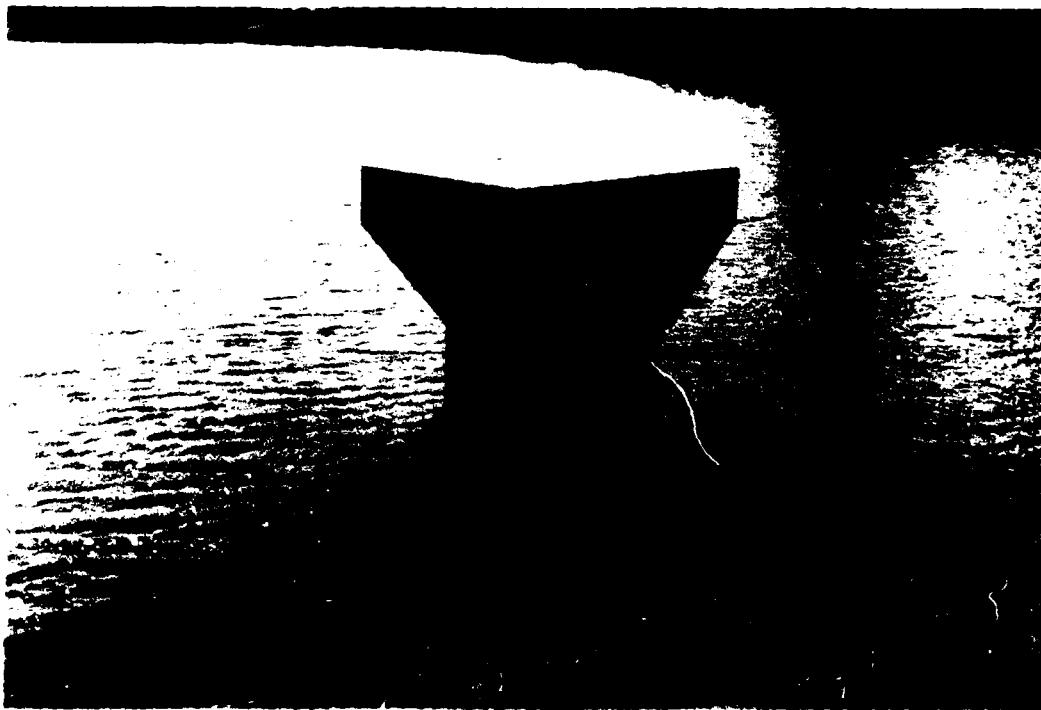
**ERICKSON, ANTHONY, ASSOCIATES
CONSULTING ENGINEERS & PLANNERS**

DATE :
MAY 1981

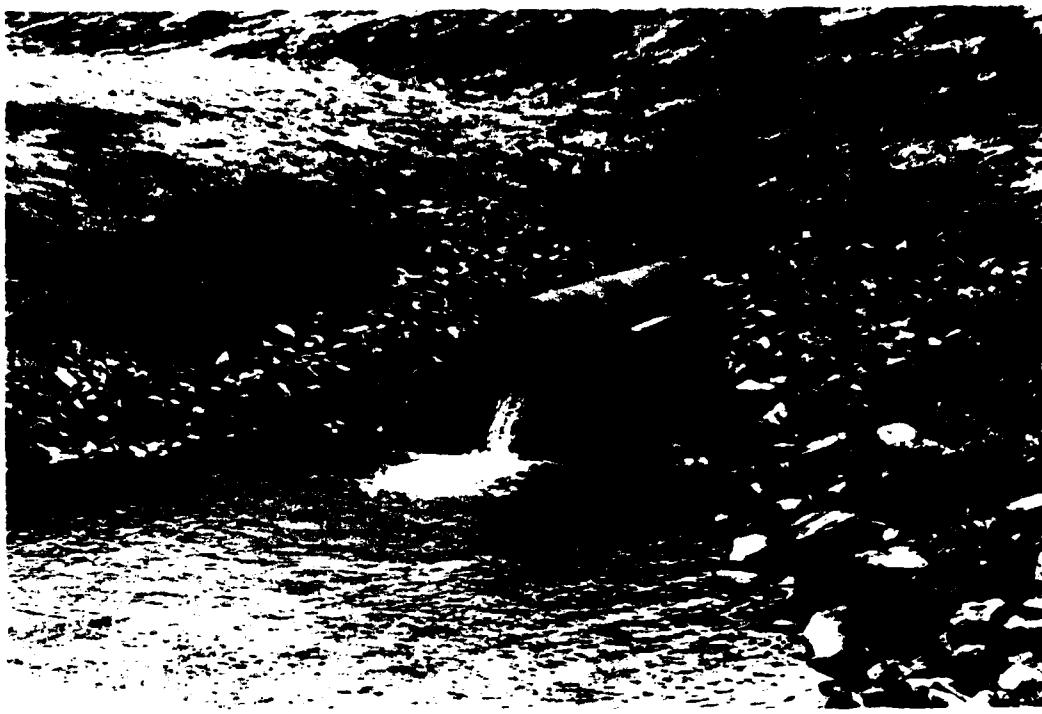
C-1



1. Principal spillway inlet structure



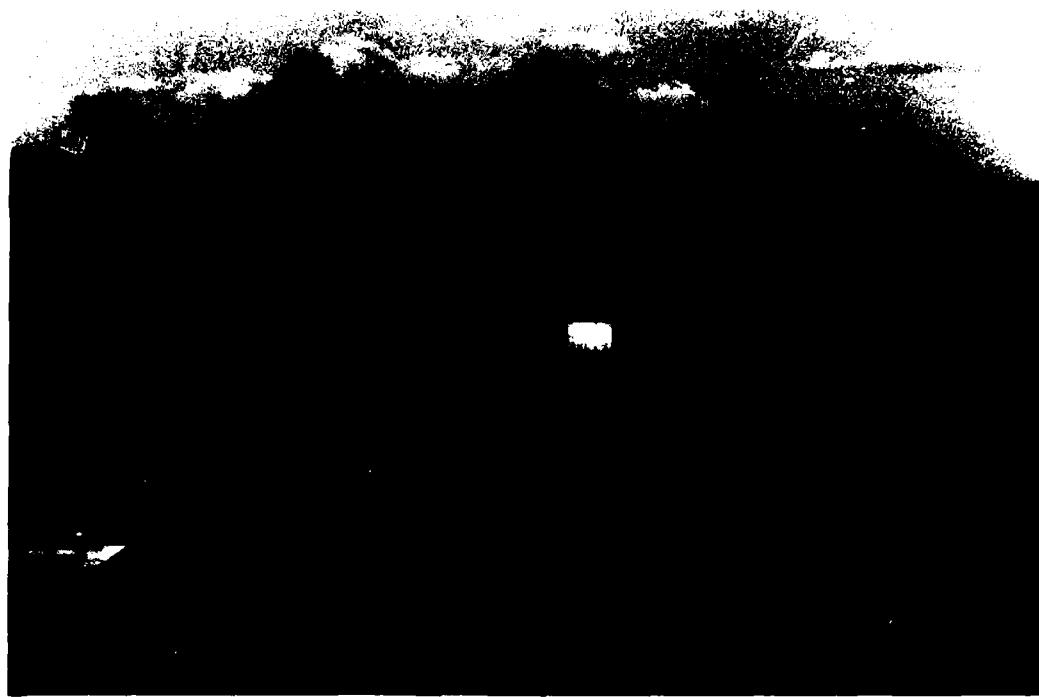
2. Principal spillway inlet structure showing low stage inlet and trash rack



3. Principal spillway outlet pipe and plunge pool



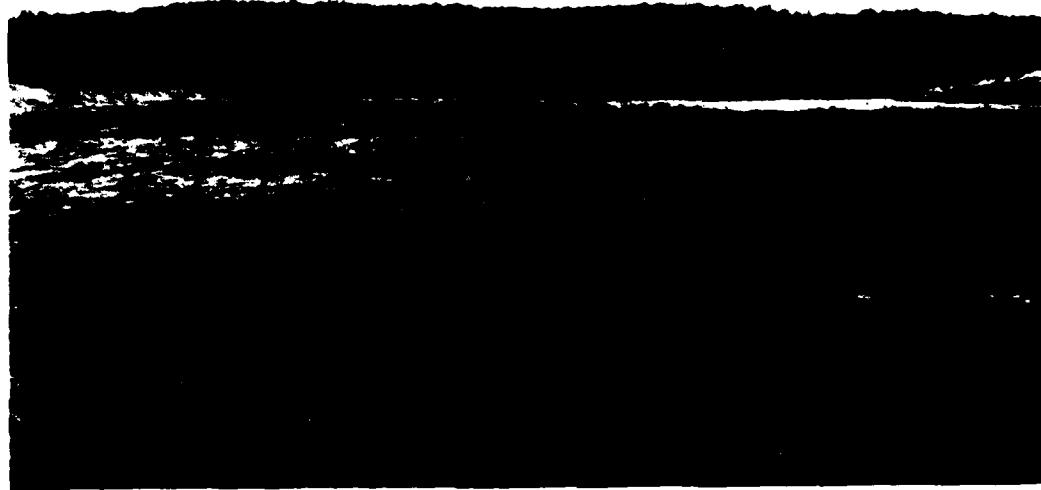
4. Plunge pool and downstream channel



5. Upstream face of dam and impoundment



6. Upstream face of dam and emergency spillway



7. Emergency spillway



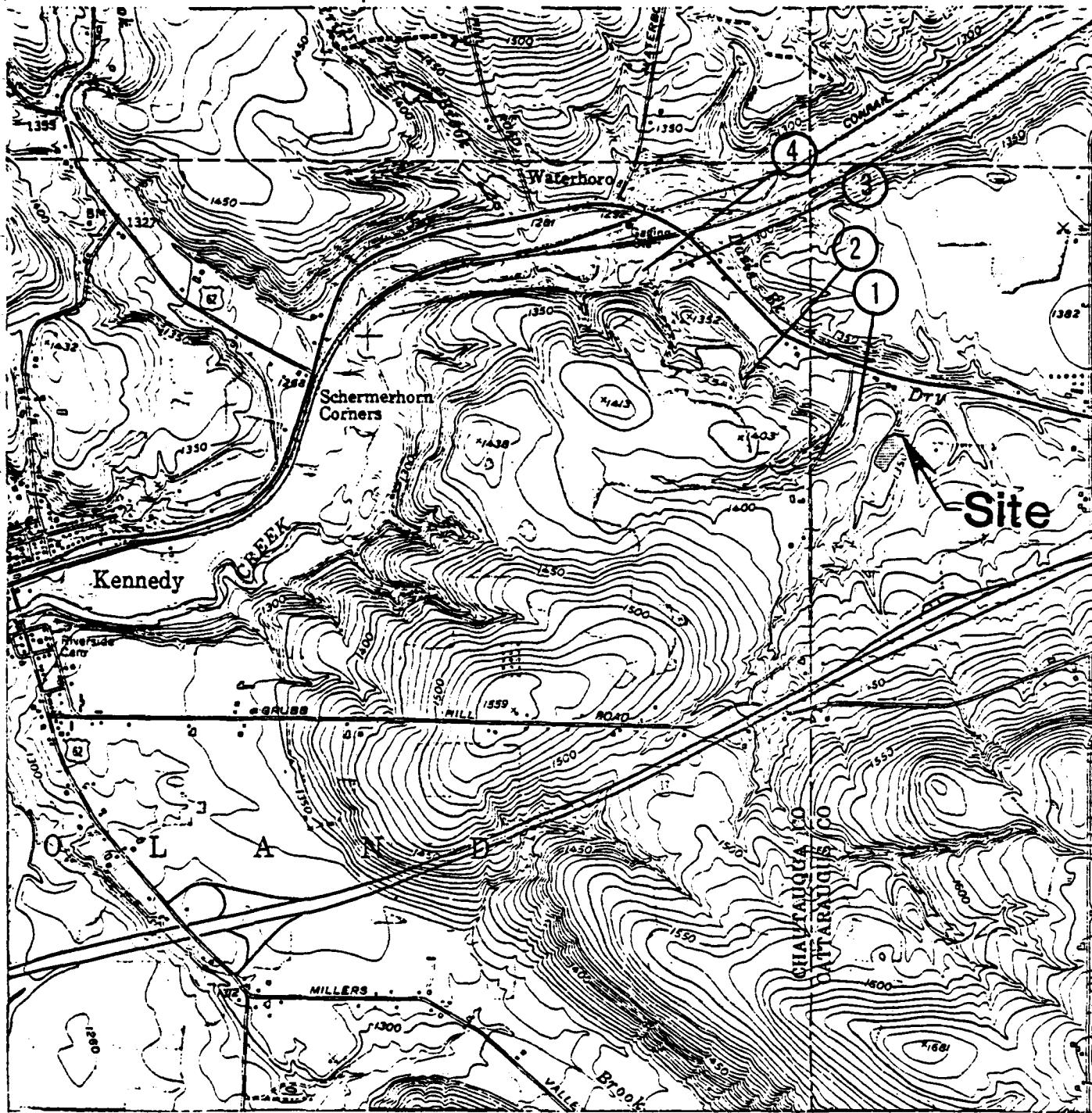
8. Aerial view

A P P E N D I X D
HYDRAULIC AND HYDROLOGIC COMPUTATIONS

APPENDIX D

PAGE

Cross Section Location Plan	D-2
HEC-1 Dam Safety Version Computer Program - Input	D-3
HEC-1 Dam Safety Version Computer Program - Output	D-4
Supporting Calculations	
● Hydrology	D-12
● Spillway Hydraulics	D-14
● Downstream Channel Routing	D-25



Davis Brook Dam (Site 1)

CROSS SECTION LOCATION PLAN

Scale: 1-2000'

D-2

A1 ANALYSIS OF DAM OVERTOPPING USING RATIOS OF PHF
 A2 HYDROLOGIC-HYDRAULIC ANALYSIS OF SAFETY OF DAVIS BROOK DAM
 A3 RATIOS OF PMF ROUTED THROUGH THE RESERVOIR AND DOWNSTREAM

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OK, SFG #HEC10B

ENTER PROJECT NUMBER
80166-00-04

-INPUT FILE? NY564

FLOOD HYDROGRAPH PACKAGE (HEC-1)

DAM SAFETY VERSION JULY 1978

LAST MODIFICATION 26 FEB 79

***** PREVIEW OF STREAM NETWORK CALCULATIONS *****

	RUNOFF HYDROGRAPH AT	INFLOW
1	ROUTE HYDROGRAPH TO	UTFLON
2	ROUTE HYDROGRAPH TO	1
3	ROUTE HYDROGRAPH TO	2
4	ROUTE HYDROGRAPH TO	3
5	ROUTE HYDROGRAPH TO	4
6	ROUTE HYDROGRAPH TO	
7	END OF NETWORK	

FLOOD HYDROGRAPH PACKAGE (HEC-1)
DAM SAFETY VERSION JULY 1978
LAST MODIFICATION 26 FEB 79

RUN DATE: 4/28/
TIME: 8:28 AM

***** ANALYSIS OF DAM OVERTOPPING USING RATIOS OF PMF *****
DAM NY 564
HYDROLOGIC-HYDRAULIC ANALYSIS OF SAFETY OF DAVIS BROOK DAM
RATIOS OF PMF ROUTED THROUGH THE RESERVOIR AND DOWNSRAMEAN

NO	NHR	NMIN	IDAY	TIR	IWIN	METRC	IPLT	IPRT	INSTAN
100	0	15	0	0	0	0	-1	4	0
			JOPER	NWTI	LROP1	TRACE			
			5	0	0	0			

MULTI-PLAN ANALYSES TO BE PERFORMED
NPLAN= 1 NRTIO= 6 LRTIO= 1
RT10S= 0.20 0.40 0.50 0.60 0.80 1.00

***** SUB-AREA RUNOFF COMPUTATION *****

CALCULATION OF INFLOW HYDROGRAPH TO RESERVOIR
ISAO ICOMP IECON IIAPE JPLI JPRT INAEV 1STAGE TAUTO
INFLOW 0 0 0 0 0 0 1 0 0

1HYUG	1WIG	TAREA	SNAP	1RSUA	1RSPC	RATIO	1SNOV	1SAME	1 LOCAL
1	1	1.60	0.00	1.60	0.00	0.000	0	1	0

SPFE PMS R6 R12 R24 R48 R72 R96
 0.00 22.80 117.00 127.00 141.00 151.00 0.00 0.00
 0.00 COMPUTED BY THE PROGRAM IS 0.000

PRECIP DATA
 LROPT STAKR DLTkr RTIOL ERAIN STKKS RTIOK STRIL CHSTL ALSMX RTIMP
 0 0.00 0.00 1.00 0.00 0.00 1.00 1.00 0.010 0.00 0.00 0.00
 LOSS DATA
 UNIT HYDROGRAPH DATA
 TP= 3.33 CP=0.63 NTA= 0

RECEDSION DATA
 STRTQ= 2.00 QRCSN= -0.10 ATIOR= 2.00

UNIT HYDROGRAPH 73 END-OF-PERIOD ORDINATES. LAG= 3.32 HOURS. CP= 0.63 VOL= 1.00
 4. 16. 32. 51. 71. 93. 116. 139. 160. 177.
 189. 196. 202. 201. 194. 180. 166. 153. 141. 130.
 119. 116. 101. 93. 86. 79. 73. 67. 62. 57.
 53. 48. 45. 41. 38. 35. 32. 30. 27. 25.
 23. 21. 20. 18. 17. 15. 14. 13. 12. 11.
 10. 9. 8. 7. 7. 6. 6. 5. 5.
 4. 4. 4. 3. 3. 3. 3. 2.
 2. 2.

END-OF-PERIOD FLOW
 MO.DA HR.MN PERIOD RAIN EXCS LOSS COMP Q MO.DA HR.PN PERIOD RAIN EXCS LOSS COMF 0
 SUH 27.54 23.79 3.7E-05971.
 (700.0)(604.0)(95.0)(2434.43)

HYDROGRAPH ROUTING

CALCULATION OF OUTFLOW HYDROGRAPH FROM RESERVOIR									
ISTAO	ICOMP	IECON	ITAPE	JPLT	JPRT	INAEV	ISAGE	IAUTO	
UTFLOW	1	0	0	0	0	1	0	0	0
GLOSS	CLOSS	Avg	IRFS	ISAME	IOPF	IPMP	LSTR		
0.0	0.000	0.00	1	1	0	0	0		
NSTPS	NSTOL	LAG	AMSKK	X	TSK	STORA	ISPRAT		
1	0	0	0.000	0.000	0.000	-1351.	-1		
STAGE	1337.70	1351.40	1356.80	1358.00	1359.00	1360.00	1361.00	1362.00	1363.00
FLOW	0.00	23.00	126.00	960.00	2201.00	3805.00	5687.00	7676.00	10276.00
CAPACITY=	23.	86.	175.	214.	273.				
ELEVATION=	1338.	1351.	1357.	1359.	1362.				
CREL	SPWIN	C00Y	IPWY	LEVEL	COOL	CARTA	EXPL		
1356.8	6.0	0.0	0.0	0.0	0.0	0.0	3.0		

		TOPEL	DAM DATA
PEAK OUTFLOW IS.	621. AT TIME 43.50 HOURS	1361.6	C900 EXPD. DANN10
PEAK OUTFLOW IS.	1301. AT TIME 43.00 HOURS	2.7	1.5 565.
PEAK OUTFLOW IS.	1626. AT TIME 43.00 HOURS		
PEAK OUTFLOW IS.	1951. AT TIME 43.00 HOURS		
PEAK OUTFLOW IS.	2604. AT TIME 43.00 HOURS		
PEAK OUTFLOW IS.	3254. AT TIME 43.00 HOURS		

HYDROGRAPH ROUTING.

CHANNEL ROUTING -MOD PULS RESERVOIR -1						
ISTAO	ICOMP	IECON	ITAPC	JPTI	JPR1	JAUTO
1	1	0	0	0	0	0
ROUTING DATA						
GLOSS	CLOSS	Avg	IRES	ISAME	IOPT	IPMP
0.0	0.000	0.00	1	1	0	0
NSTPS	NSTOL	LAG	AHSKK	X	TSK	SITRA
1	0	0	0.000	0.000	0	ISPRAT
					0.	0.

NORMAL DEPTH CHANNEL ROUTING

QN(1)	QN(2)	QN(3)	FLNWT	FLMAX	FLNTH	SEL
0.0450	0.0500	0.0450	1298.0	1350.0	1600.	0.04000

CROSS SECTION COORDINATES--STA.ELEV--STA.ELEV--LIC						
0.00	1350.00	900.00	1320.00	742.50	1305.00	752.50
782.50	1305.00	950.00	1320.00	1025.00	1350.00	1298.00
						772.50
						1298.00

STORAGE	2H7.0H	2.40	5.59	10.41	23.24	45.43	76.97	117.87	168.12	221.42
OUTFLOW	277066.00	662.66	2246.87	5100.31	11732.69	25084.71	47587.94	81348.67	128278.72	155471.38
STAGE	1298.00	1300.74	1303.47	1306.21	1308.95	1311.68	1314.42	1317.16	1319.89	1321.63
FLOW	277066.00	662.66	2246.87	5100.31	11732.69	25084.71	47587.94	81348.67	128278.72	155471.38

MAXIMUM STAGE IS 1300.6
 MAXIMUM STAGE IS 1301.8
 MAXIMUM STAGE IS 1302.4
 MAXIMUM STAGE IS 1303.0
 MAXIMUM STAGE IS 1303.6
 MAXIMUM STAGE IS 1304.4

HYDROGRAPH ROUTING

CHANNEL ROUTING -MOD PULS REACH 1-2

	ISTAO	ICOMP	ITECN	ITAPE	JPLT	JPRI	INAPE	ISSTAGE	IAUTO
ROUTING DATA	2	1	0	0	0	0	1	0	0
GLOSS	CLOSS	Avg	IRES	ISAME	10PI	IPMP			
0.9	0.000	0.00	1	1	0	0			
NSTPS	NSTOL	LAG	AMSKK	X	TSK	STORA	ISPRAT		
1	0	0	0.000	0.000	0.000	0.000			

NORMAL DEPTH CHANNEL ROUTING

DN(1) DN(2) DN(3) ELNVT ELMAX RLNTH SEL
 0.0750 0.0500 0.0750 1287.0 1310.0 1100. 0.01000

CROSS SECTION COORDINATES--STA,ELEV,STA,ELEV--EFC

0.00 1310.00 100.00 1300.00 582.00 1294.00 597.00 1287.00 617.00 1287.00

632.00 1294.00 700.00 1300.00 890.00 1310.00

STORAGE	OUTFLOW	STAGE	FLOW	MAXIMUM STAGE IS	MAXIMUM STAGE IS
0.00 42.79	0.00 11077.67	1287.00 1299.10	11077.67	1290.7	1292.5
0.69 60.24	84.89 16017.80	1288.21 1300.31	1289.42 1301.53	262.54 2233.38	262.54 2233.38
1.54 79.39	584.92 30727.40	1290.63 1302.74	1291.84 1303.95	99.62 39976.66	99.62 39976.66
2.55 99.62	996.47 50474.09	1291.84 1305.16	1294.26 1306.37	1624.14 62221.90	1624.14 62221.90
3.71 120.92	1624.14 50474.09	1294.26 1306.37	1295.47 1307.58	2288.94 75228.27	2288.94 75228.27
5.04 143.30	2288.94 62221.90	1295.47 1307.58	1296.68 1308.79	3296.75 89505.47	3296.75 89505.47
6.60 166.75	3296.75 89505.47	1296.68 1308.79	1297.28 1310.80	4987.28 15066.61	4987.28 15066.61
10.56 191.27	4987.28 15066.61	1297.28 1310.80	1297.28 1310.80	7514.82 15066.61	7514.82 15066.61
11.91 216.86	7514.82 15066.61	1297.28 1310.80	1297.28 1310.80	24.53 24.53	24.53 24.53

MAXIMUM STAGE IS 1293.2
 MAXIMUM STAGE IS 1293.8
 MAXIMUM STAGE IS 1294.7
 MAXIMUM STAGE IS 1295.4

HYDROGRAPH ROUTING

CHANNEL ROUTING -MOD PULS REACH 2-3
 ISTAO ICOMP IECON ITAPE JPLI JPRT INAME I1STAGE IAUTO
 3 1 0 0 0 0 0 0 0
 ROUTING DATA
 QLOSS CLOSS AVG IRES ISAME IOPT IPHP LSIR
 0.0 0.000 0.00 0.00 1 1 0 0 0
 NSTPS NSTDL LAG AMSIK X TSK STORA ISPRAT
 1 0 0 0.000 0.000 0.000 0.000 0.0

NORMAL DEPTH CHANNEL ROUTING

DN(1)	DN(2)	QN(3)	ELNVT	ELMAX	RLNTH	SEL
0.0750	0.0500	0.0750	1262.0	1275.0	1700.	0.01500

CROSS SECTION COORDINATES--STA,ELEV,STA,ELEV--FTC 735.00 1262.00

0.00	1275.00	300.00	1270.00	700.00	1269.00	715.00	1262.00	735.00	1262.00
750.00	1269.00	850.00	1270.00	950.00	1275.00				
STORAGE	0.00	0.57	1.22	1.95	2.76	3.65	4.61	5.66	6.78
	9.25	13.27	25.82	41.68	59.01	77.79	96.03	119.74	142.98
OUTFLOW	0.00	39.47	128.25	258.82	430.06	642.43	897.04	1195.33	1530.90
	2368.67	3004.79	4255.19	6355.04	9136.22	12574.61	16668.92	21421.97	26865.85
STAGE	1262.00	1262.68	1263.37	1264.05	1264.74	1265.42	1266.10	1266.79	1267.47
	1268.04	1269.52	1270.21	1270.89	1271.58	1272.26	1272.95	1273.63	1274.31
FLOW	0.00	39.47	128.25	258.82	430.06	642.43	897.04	1195.33	1530.90
	2368.67	3004.79	4255.19	6355.04	9136.22	12574.61	16668.92	21421.97	26865.85
MAXIMUM STAGE IS									
MAXIMUM STAGE IS	1267.0								
MAXIMUM STAGE IS	1267.6								
MAXIMUM STAGE IS	1268.2								

OK • SEC 1118

PAGE 6006

MAXIMUM STAGE IS 1269.1 MAXIMUM STAGE IS 1269.7

HYDROGEN BONDING

NORMAL GEPTH CHANNEL ROUTING

CROSS SECTION COORDINATES--STA-ELEV STA-ELEV-ETC					
0.00	1278.00	205.00	1260.00	215.00	245.00
300.00	1278.00	301.00	1270.00	320.00	320.00
STORAGE	0.00	0.27	0.57	0.90	1.25
	4.90	6.04	7.34	8.62	10.47
OUTFLOW	0.00	75.46	245.02	492.71	814.36
	4489.36	5708.04	7189.16	8958.86	11042.13
STAGE	1255.00	1255.79	1256.58	1257.37	1258.16
	1262.89	1263.68	1264.47	1265.26	1266.05
FLOW	0.00	75.46	245.02	492.71	814.36
	4489.36	5708.04	7189.16	8958.86	11042.13

MAXIMUM STAGE IS	1257.7
MAXIMUM STAGE IS	1259.1
MAXIMUM STAGE IS	1259.6
MAXIMUM STAGE IS	1260.2
MAXIMUM STAGE IS	1261.1
MAXIMUM STAGE IS	1261.8

PEAK FLOW AND STORAGE (END OF PERIOD) SUMMARY FOR MULTIPLE PLAN-RATIO ECONOMIC COMPUTATIONS
 FLOWS IN CUBIC FEET PER SECOND (CUBIC METERS PER SECOND)
 AREA IN SQUARE MILES (SQUARE KILOMETERS)

OPERATION	STATION	AREA	PLAN	RATIOS APPLIED TO FLOWS					
				RATIO 1	RATIO 2	RATIO 3	RATIO 4	RATIO 5	RATIO 6
				0.20	0.40	0.50	0.60	0.80	1.00
HYDROGRAPH AT INFLOW	1.60 (4.14)		1 652. (18.47)	1305. (36.94)	1631. (46.17)	1957. (55.41)	2699. (73.88)	3261. (92.35)	
ROUTED TO OUTFLOW	1.60 (4.14)		1 621. (17.58)	1301. (36.84)	1626. (46.04)	1951. (55.25)	2699. (73.72)	3254. (92.15)	
ROUTED TO	1 (4.14)		1 623. (17.64)	1300. (36.80)	1625. (46.03)	1951. (55.23)	2692. (73.69)	3254. (92.14)	
ROUTED TO	2 (4.14)		1 619. (17.53)	1302. (36.86)	1626. (46.03)	1959. (55.18)	2692. (73.67)	3251. (92.07)	
ROUTED TO	3 (4.14)		1 622. (17.60)	1298. (36.76)	1623. (45.94)	1948. (55.16)	2598. (73.56)	3246. (91.93)	
ROUTED TO	4 (4.14)		1 622. (17.61)	1300. (36.81)	1620. (45.98)	1948. (55.15)	2597. (73.55)	3246. (91.92)	

SUMMARY OF DAM SAFETY ANALYSIS

PLAN 1	INITIAL VALUE	SPILLWAY CREST	TOP OF DAM	MAX OUTFLOW	TIME OF FAILURE
	1351.40	1356.80	1361.60		
	86.	175.	273.		
	23.	126.	700.		
RATIO OF PFM	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	DURATION OVER TOP	HOURS	HOURS
W.S. ELEV		CFS			
0.20	1357.51	0.00	188.	621.	0.00
0.40	1358.27	0.00	202.	1301.	0.00
0.50	1358.54	0.00	207.	1626.	0.00
0.60	1358.60	0.00	212.	1951.	0.00
0.80	1359.25	0.00	221.	2604.	0.00
1.00	1359.66	0.00	230.	3254.	0.00

PLAN 1 STATION 1
 MAXIMUM TIME

RATIO	FLOW, CFS		STAGE, FT		TIME	
	MAXIMUM	FLOW, CFS	STAGE, FT	MAXIMUM	STAGE, FT	TIME
0.20	623.	1300.6	43.50	0.20	1301.0	43.00
0.40	1300.	1301.0	43.00	0.40	1302.4	43.00
0.50	1625.	1303.0	43.00	0.50	1303.0	43.00
0.60	1951.	1303.0	43.00	0.60	1303.8	43.00
0.80	2602.	1303.8	43.00	0.80	1304.4	43.00
1.00	3254.	1304.4	43.00			

PLAN 1 STATION

RATIO	FLOW, CFS		STAGE, FT		TIME	
	MAXIMUM	FLOW, CFS	STAGE, FT	MAXIMUM	STAGE, FT	TIME
0.20	619.	1290.7	43.50	0.20	1292.5	43.00
0.40	1302.	1293.2	43.00	0.40	1293.8	43.00
0.50	1626.	1294.4	43.00	0.50	1295.0	43.00
0.60	1949.	1295.6	43.00	0.60	1296.2	43.00
0.80	2602.	1297.0	43.00	0.80	1297.6	43.00
1.00	3251.	1298.4	43.00			

PLAN 1 STATION

RATIO	FLOW, CFS		STAGE, FT		TIME	
	MAXIMUM	FLOW, CFS	STAGE, FT	MAXIMUM	STAGE, FT	TIME
0.20	622.	1265.4	43.75	0.20	1267.0	43.25
0.40	1298.	1267.6	43.25	0.40	1268.2	43.00
0.50	1623.	1268.8	43.00	0.50	1269.1	43.00
0.60	1948.	1269.4	43.00	0.60	1269.7	43.00
0.80	2598.	1270.1	43.00	0.80	1270.4	43.00
1.00	3246.	1270.7	43.00			

PLAN 1 STATION

RATIO	FLOW, CFS		STAGE, FT		TIME	
	MAXIMUM	FLOW, CFS	STAGE, FT	MAXIMUM	STAGE, FT	TIME
0.20	622.	1257.7	43.75	0.20	1259.1	43.25
0.40	1300.	1260.2	43.25	0.40	1260.7	43.00
0.50	1624.	1261.1	43.00	0.50	1261.6	43.00
0.60	1948.	1262.1	43.00	0.60	1262.6	43.00
0.80	2597.	1263.1	43.00	0.80	1263.6	43.00
1.00	3246.	1264.1	43.00			

DATE 3/16/87 ERDMAN, ANTHONY, ASSOCIATES SHEET 1 OF 1
 B.R. DATE 3/16/87 SUBJECT DLM 564 HYDROLOGY SUB-SHEET NO. 1
 OWNER PROJECT NAME HEC-10B DAM INSPECTION 80166-00-05

DAM 564 DAVIS BROOK DAM

REF. QUAD. KENNEDY, N.Y.

DISTANCE L & L_{ca} MEASURED BY MAP MEASURING WHEEL (1" = 2000')

COMPUTATIONS FOR L DISTANCE

RUN	MEAS. DIST.	Avg. Dist.	COEF.	L-DISTANCE
A	1 = 7.9"			
	<u>2 = 8.0</u>			
	15.9"	÷ 2 = 7.95"	× 2000'	= 15900 FT.

* L = 15900 FT.

COMPUTATIONS FOR L_{ca} DISTANCE

RUN	MEAS. DIST.	Avg. Dist.	COEF.	L _{ca} DISTANCE
A	1 = 4.3"			
	<u>2 = 4.4</u> "			
	8.7"	÷ 2 = 4.35"	× 2000'	= 8700 FT.

* L_{ca} = 8700 FT.

DATE 3/17/81 ERDMAN, ANTHONY, ASSOCIATES SHEET - 1 -
 SUBJECT DAVIS 564 HYDROLOGY SUB-SHEET NO. 2
 PROJECT NAME DAVIS BROOK DAM (90166-00.05)

$$\tau_p = C_T (L L_{ea})^{0.3} \quad , \quad C_T = 2.00$$

$$\tau_r = \frac{\tau_p}{5.5} \quad , \quad C_p = 0.63$$

$$\tau_{pr} = \tau_p + 0.25(\tau_r - \tau_r)$$

$$L = 15900' = 3.01 \text{ mi}$$

$$L_{ea} = 8700' = 1.65 \text{ mi}$$

$$\tau_p = 2(3.01 \times 1.65)^{0.3} = 3.23 \text{ hr. } \checkmark$$

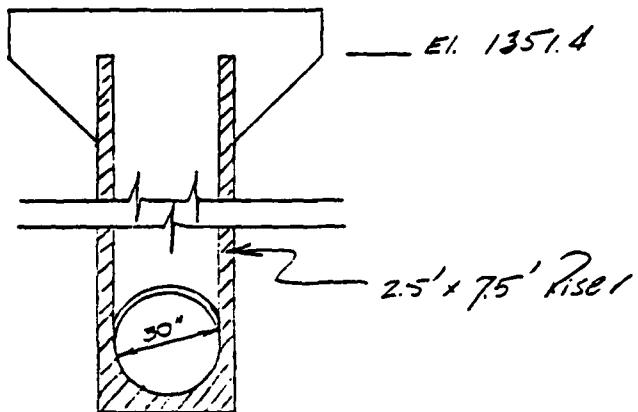
$$\tau_r = \frac{3.23}{5.5} = 0.59 \text{ hr} \implies \tau_r = 1.0 \text{ hr.}$$

$$\tau_{pr} = 3.23 + 0.25(1 - 0.59) = 3.33 \text{ hr.}$$

DATE 5/17/81 ERDMAN, ANTHONY, ASSOCIATES SHEET 2 OF 15
 B.R. DATE 5/17/81 SUBJECT DAI = 54 - Hydroline's SUB-SHEET NO. 1
 OWNER PROJECT NAME DAI INSPECTIONS (80166-05.05)

Service Spillway

Assume that the 30° CCP is the control & develop an eqn. of the form $Q = CA\sqrt{2gH}$ to describe the flow.



From Design Report

$$Q_s = 23 \text{ cfs} @ \text{EL. } 1351.4$$

$$A_o = \pi(1.25)^2 = 4.9 \text{ ft}^2 \quad \checkmark$$

$$Q_s = 126 \text{ cfs} @ \text{EL. } 1356.8$$

Determine C_o from $Q_s = 126 \text{ cfs}$ & $Q_s = 23 \text{ cfs}$

$$H_o = 1356.8 - 1351.4 = 5.4$$

$$C_o = \frac{Q_s}{A_o \sqrt{2gH_o}} = \frac{126 \text{ cfs} - 23 \text{ cfs}}{4.9 \sqrt{2(32.2)(5.4)}} = 1.13 \quad \checkmark$$

$$Q_s = 1.13 / (4.9 \text{ ft}^2) / \sqrt{2(32.2)} H_o^{0.5} + 23 \text{ cfs} = 44.43 H_o^{0.5} + 23$$

$$Q_s = 44.43 H_o^{0.5} + 23 \quad \checkmark$$

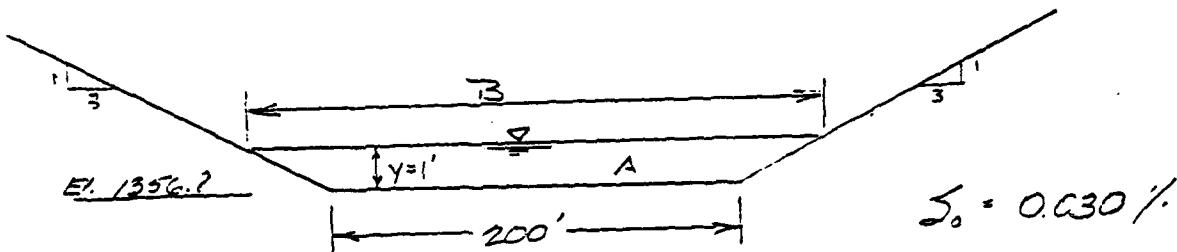
Elev.	H_o	Q_s	
1356.8	5.4	126	✓
1358.0	6.6	137	✓
1359.0	7.6	145	✓
1360.0	8.6	153	✓
1361.0	9.6	161	✓
1362.0	10.6	168	✓
1363.0	11.6	174	✓
1364.0	10.2	165	✓

Emergency Spillway

Ref: "Broter & King" Table 8-7 pg. 8-59

Determining the Discharge Q of a Trapezoidal Channel when the flow is at Critical Depth

Check to see if flow passes through critical depth.
 Determine critical slope for a flow depth of $y = 1.0'$. If
 Spillway slope $>$ critical slope, then flows pass through
 the critical depth and Table 8-7 holds



$$\text{Critical depth flow } \frac{Q_c}{g} = \frac{A^2}{B} \Rightarrow Q_c = \sqrt{g A^2}$$

For $y = 1.0'$

$$A = 200'(1') + 2(1/2 \times 3 \times 1') = 203 \text{ ft}^2 \quad \checkmark$$

$$B = 200' + 2(3 \times 1') = 206 \text{ ft} \quad \checkmark$$

$$Q_c = \sqrt{\frac{32.2(203 \text{ ft}^2)^3}{206}} = 1144 \text{ cfs} \quad \checkmark$$

DATE 5/17/81 ERDMAN, ANTHONY, ASSOCIATES SHEET 5 OF 15
 B.R. DATE 5/17/81 SUBJECT T-203-74 - Hydraulics SUB-SHEET NO. 3
 OWNER PROJECT NAME T-203-74 INSPECTIONS (50416-60.05)

$$K = \frac{149}{n} AR^{\frac{2}{3}} = \frac{149}{0.03} \left(\frac{203.4^2}{206.32} \right)^{\frac{2}{3}} = 9974 \checkmark$$

$n = 0.030$ for Earth, fairly uniform section of grass f. some ripples.

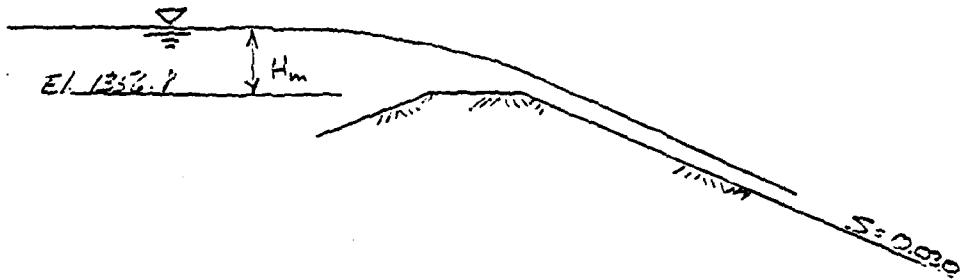
$$S_c = \left(\frac{Q_c}{K} \right)^2 = \left(\frac{1144}{9974} \right)^2 = 0.013 \checkmark$$

Spillway slope \geq critical slope
 $0.030 \geq 0.013 \therefore$

flow passes through the critical depth for $y=10'$ and
 also for $y > 10'$. Use Table 8-7.

$$\bar{z} = 3/1 = 3.0$$

$$b = 200 \text{ ft}$$



Elev	H_m	$H_m^{\frac{2}{3}}/b$	C_2	Q_c
1356.7	0	0	0	0
1358.0	1.2	.018	3.13	823
1359.0	2.2	.033	3.15	2,056
1360.0	3.2	.048	3.19	3,652
1361.0	4.2	.063	3.21	5,526
1362.0	5.2	.078	3.25	7,708
1363.0	6.2	.093	3.27	10,096

$$Q_c = C_2 b H_m^{1.5} \checkmark$$

$$1361.6 \quad 4.8 \quad .072 \quad 3.23 \quad 6794 \checkmark$$

BY P.E. DATE 3/26/51 ERDMAN, ANTHONY, ASSOCIATES SHEET 6 OF 10
 C JOB DATE 3/31/51 SUBJECT DAM 564 RESERVOIR AREA SUB-SHEET NO. 4
 OWNER PROJECT NAME HEC-1 DAM INSPECTION 60166-00-05

DAVIS BROOK DAM

$\$A$ = RAREA RESERVOIR SURFACE AREA IN ACRES

$\$E$ = RELEV RESERVOIR ELEVATION IN FEET.

REF. U.S. DEPT. OF A.S.C.A. AS BUILT PLAK Dwg. NY-2155-P

SCALE 1" = 200 ('1/2 REDUCTION SCALE 1" = 400')

$$\text{Eq. } \text{in}^2 \times \frac{400 \text{ ft}^2}{\text{in}^2} \times \frac{1 \text{ ac.}}{43560 \text{ ft}^2} = \text{ac.}$$

ELEV. 1337.7 = 4.1 AC GIVEN DESIGN REPORT sh.4

$$\text{ELEV. } 1345 = 2.40 \text{ in}^2 \times \frac{400 \text{ ft}^2}{\text{in}^2} \times \frac{1 \text{ ac.}}{43560 \text{ ft}^2} = 8.82 \text{ ac.}$$

ELEV. 1351.4 = 13.8 AC GIVEN DESIGN REPORT sh.4

ELEV. 1356.8 = 17.8 AC GIVEN DESIGN REPORT sh.4

ELEV. 1358.9 = 20.0 AC GIVEN DESIGN REPORT sh.4

ELEV. 1361.6 = 22.8 AC GIVEN DESIGN REPORT sh.4

$$\text{ELEV. } 1365 = 7.40 \text{ in}^2 \times \frac{400 \text{ ft}^2}{\text{in}^2} \times \frac{1 \text{ ac.}}{43560 \text{ ft}^2} = 27.18 \text{ ac.}$$

NOTE: The stage-storage from the SCS design report.
was used.

DATE - - - - - ERDMAN, ANTHONY, ASSOCIATES SHEET 1 OF 15
B.R. DATE 5/7/81 SUBJECT DAM = 564-Hydraulics SUB-SHEET NO. 5
OWNER PROJECT NAME DAM INSPECTION 180166-00.05

Total Spillway DISCHARGE ($Q_s + Q_e$)

ELEV.	$Q_3 + Q_{\bar{E}}$	Reservoir Surface Area	
1337.7	0	4.1	✓
1345.0	—	8.8	✓
1351.4	23	13.8	✓
1356.8	126	17.8	—
1358.0	960	—	—
1358.9	—	20.0	✓
1359.0	2,201	—	—
1360.0	3,805	—	—
1361.0	5,687	—	—
1361.6	6,959	22.8	✓
1362.0	7,876	—	—
1363.0	10,270	—	—
1365.0	—	27.2	✓

AD-A105 841 ERDMAN ANTHONY ASSOCIATES ROCHESTER NY
NATIONAL DAM SAFETY PROGRAM. DAVIS BROOK DAM (SITE 1) (INVENTOR--ETC(U)
AUG 81 R J FARRELL DACW51-81-C-0017 NL

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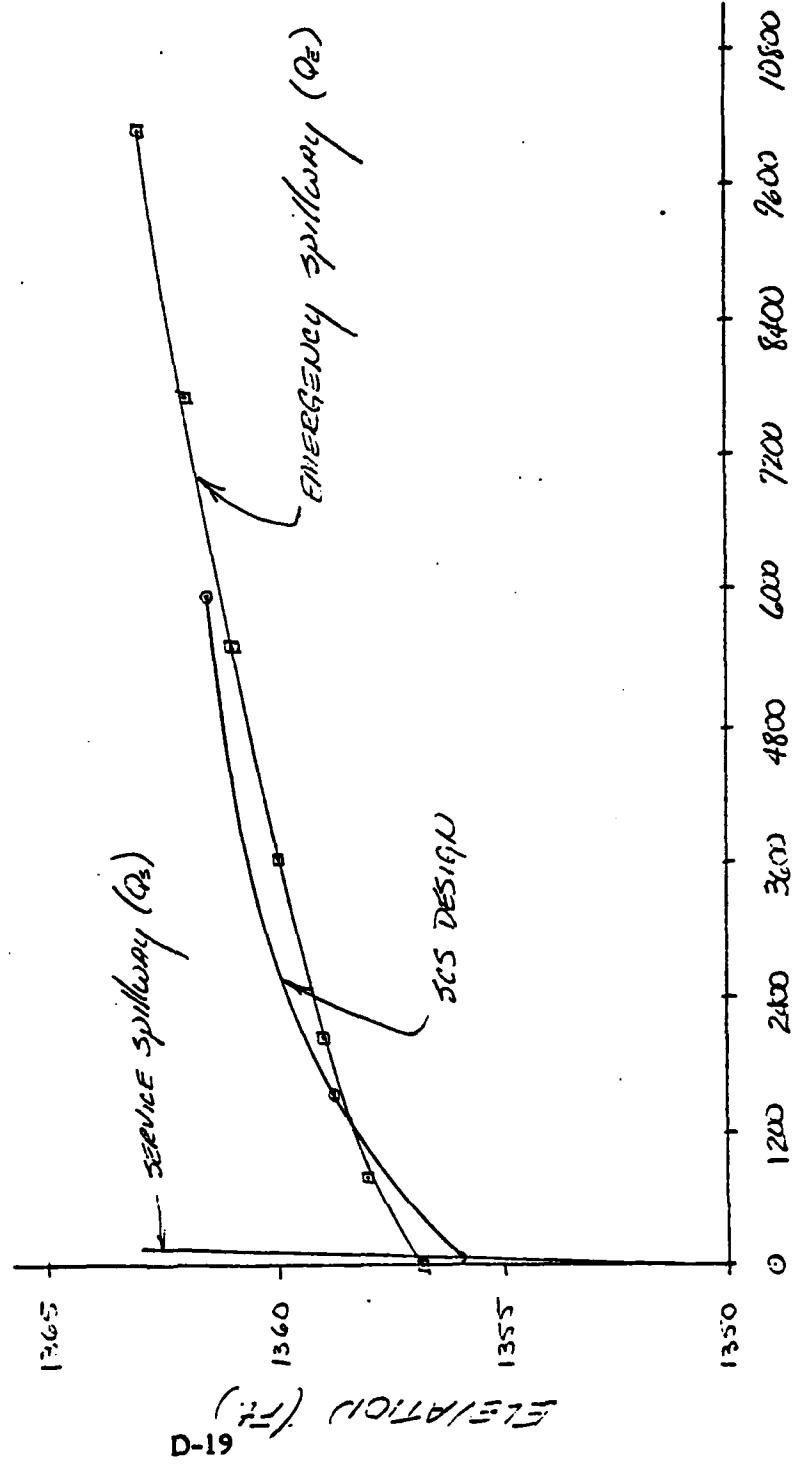
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DATE FILMED
11-81
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DATE 5/7/81 SUBJECT D-19 - 5th - Hairpin Curves SHEET 5 OF 15
 L.R. DATE 5/7/81 SUBJECT D-19 - 5th - Hairpin Curves SUB-SHEET NO. 6
 OWNER PROJECT NAME INSPECTIONS 1/5 (PA 66-03.05)

Spillway Rating Curve - Day 561



B.R. DATE 5/7/81 SUBJECT D11:11 - 564-
OWNER PROJECT NAME DAM SIDECTIONS (80166-SD.05)

SHEET

1 OF 15

SUB-SHEET NO. 7

Overtopping Data

Dam Height = 1361.6 ✓

Discharge Coefficient (C) = 2.7

Exponent (E) = 1.5

Length of Dam Crest = 564.6 ✓

DATE 5/7/81 ERDMAN, ANTHONY, ASSOCIATES SHEET 10 OF 15
 C.R. SUBJECT DAM 564 - Hydroanilis SUB-SHEET NO. 8
 OWNER PROJECT NAME DAM INSPECTIONS (80163-7.05)

Estimated 5,2: Hwy Capacity @ Tolt Fld (E7. 1359.7)

	ELEV.	Q	
Principal	1359.0	145	✓
	1360.0	153	✓
Emergency	1359.0	2,056	✓
	1360.0	3,652	✓

Principal Cap @ 1359.7

$$\frac{1.0}{8} = \frac{0.7}{x} \quad x = 5.6$$

Capacity = 145 + 5.6 = 150.6 cfs Say 151 cfs ✓

Emergency Cap. @ 1359.7

$$\frac{1.0}{1596} = \frac{0.7}{x} \quad x = 1117.2$$

Capacity = 2,056 + 1117.2 = 3173.2 Say 3,173 cfs -

Q_{Total} (from HEC I) = 3254 cfs

- $Q_{Principal}$ = 151 cfs

$Q_{Emergency}$ = 3103 cfs ✓

8 DATE 5-17-81
CNR R.R. DATE 5-17-81
OWNER

ERDMAN, ANTHONY, ASSOCIATES

SUBJECT DAM 52A - Hydraulics
PROJECT NAME DAM INSPECTION (80116-80.05)

SHEET 11 OF 15

SUB-SHEET NO. 9

Reservoir Surface Area @ 1st Flood (El 1359.1)

EPL
1358.9

SP
20.0

1361.6 22.8

$$\frac{2.7}{2.8} = \frac{0.1}{x} \quad x = 0.83$$

$$SA = 20.83 \text{ acres} \quad \checkmark$$

K.L.D. DATE 5/1/81 ERDMAN, ANTHONY, ASSOCIATES SHEET 12 OF 15
 C.R. DATE 5/1/81 SUBJECT DAM #324 - HYDRAULICS SUB-SHEET NO. 10
 OWNER PROJECT NAME DAM INSPECTION (80166-01.05)

Emergency Spillway Capacities

Flood	Q _{TOTAL}	Elev.	Q _{es}	A	V	Comments
PMF	3254	1359.66	3103	446	7.0	<8.0 no erosion
MF	1626	1358.54	1489	284	5.2	<8.0 no erosion

PMF

$$\text{Assume } \frac{y_n}{b} < 0.02 \Rightarrow \therefore y_n = 0.789 \left(\frac{Q_n}{b S_0^{0.5}} \right)^{0.6}$$

$$y_n = 0.789 \left(\frac{3103(0.06)}{200(0.03)^{0.5}} \right)^{0.6} = 2.16' \checkmark \quad \frac{y_n}{b} = \frac{2.16}{200} = 0.01 < 0.02 \underline{\text{OK}}$$

$$A = (2.16)(200) + 2\left(\frac{1}{2}(2.16)(3)(2.16)\right) = 446 \text{ ft}^2 \checkmark$$

$$V = \frac{Q}{A} = \frac{3103}{446} = \underline{\underline{7.0 \text{ ft/sec}}} \checkmark$$

in PMF

$$\begin{array}{lll} \text{Elev} & \frac{Q}{E} & \\ \hline 1358 & 823 & Q_{1358.54} = 823 \text{ cfs} + .54(2056 - 823) = 1489 \text{ cfs} \\ 1359 & 2056 & \end{array}$$

Assuming $\frac{y_n}{b} < 0.02$

$$y_n = 0.789 \left(\frac{1489(0.06)}{200(0.03)^{0.5}} \right)^{0.6} = 1.39' \checkmark \quad \frac{y_n}{b} = 0.007 < 0.02 \underline{\text{OK}}$$

$$A = (1.39')(200') + 2\left(\frac{1}{2}(1.39')(3)(1.39')\right) = 284 \text{ ft}^2 \checkmark$$

$$V = \frac{Q}{A} = \frac{1489}{284} = \underline{\underline{5.2 \text{ ft/sec}}} \checkmark$$

DATE 5/15 DATE 5/12/81 SUBJECT Dm 564 - Hydraulics
SUB-SHEET NO. 11
PROJECT NAME Dm Inspections (E0166-00.C5)

DAVIS BROOK DAM - STAGE vs STORAGE RELATIONSHIP

Elevation

1337.7
1351.4
1356.8
1358.9
1361.6

Storage

23.3'
85.8'
174.8'
213.5'
273.0'

Ref: SCS design report

D.E.W. DATE 3-20-81 ERDMAN, ANTHONY, ASSOCIATES SHEET 14 OF 15
 CAD B.R. DATE 3/21/81 SUBJECT DAM 564 ROUTING SUB-SHEET NO. 1
 PROJECT NAME DAM INSPECTION SO166-00-05
 B.R. 4/13/81
 XRA 4/13/81 DAVIS BROOK DAM

DAM DATA FROM AS BUILT PLAN

DAM TOP ELEV. 1361.7

DAM INV. 1316.2

$\frac{1350}{0}$	$\frac{1320}{400}$	$\frac{1305}{742.5}$	$\frac{1298}{752.5}$	$\frac{1298}{772.5}$	$\frac{1305}{782.5}$	$\frac{1320}{950}$	$\frac{1350}{1025}$
------------------	--------------------	----------------------	----------------------	----------------------	----------------------	--------------------	---------------------

REACH 1 LENGTH = 1600'

CROSS SECT. $\frac{1350}{5}$ $\frac{1320}{400}$ $\frac{1300}{750}$ $\frac{1295}{760}$ $\frac{1295}{765}$ $\frac{1300}{775}$ $\frac{1320}{950}$ $\frac{1350}{1025}$

SLOPE: DAM INV. - REACH 1 INV. = $h \div L$ = SLOPE

$$1316.2 - 1298 = 63.2 \div 1600' = 0.0400$$

REACH 2 LENGTH = 1100' $\frac{1310}{0}$, $\frac{1300}{100}$, $\frac{1294}{582}$, $\frac{1287}{597}$, $\frac{1287}{617}$, $\frac{1294}{632}$, $\frac{1300}{700}$, $\frac{1310}{890}$

CROSS SECT. = $\frac{1310}{8}$ $\frac{1300}{100}$ $\frac{1290}{575}$ $\frac{1287}{602}$ $\frac{1287}{612}$ $\frac{1290}{640}$ $\frac{1300}{700}$ $\frac{1310}{890}$

SLOPE: REACH 1 INV. - REACH 2 INV. = $h \div L$ = SLOPE

$$1298 - 1287 = 11' \div 1100' = 0.010$$

REACH 3 LENGTH = 1700' $\frac{1275}{0}$, $\frac{1270}{300}$, $\frac{1269}{700}$, $\frac{1262}{715}$, $\frac{1262}{735}$, $\frac{1269}{750}$, $\frac{1270}{850}$, $\frac{1275}{950}$

CROSS SECT. $\frac{1275}{0}$ $\frac{1270}{300}$ $\frac{1270}{600}$ $\frac{1262}{720}$ $\frac{1262}{730}$ $\frac{1270}{850}$ $\frac{1275}{950}$

SLOPE: REACH 2 INV. - REACH 3 INV. = $h \div L$ = SLOPE

$$1287 - 1262 = 25 \div 1700' = 0.015$$

REACH 4 LENGTH = 475'

CROSS SECT. $\frac{1270}{0}$ $\frac{1260}{200}$ $\frac{1255}{225}$ $\frac{1255}{235}$ $\frac{1260}{265}$ $\frac{1270}{300}$

SLOPE: REACH 3 INV. - REACH 4 INV. = $h \div L$ = SLOPE

$$1262 - 1255 = 7 \div 475' = 0.015$$

$\frac{1270}{0}$, $\frac{1260}{205}$, $\frac{1255}{215}$, $\frac{1255}{245}$, $\frac{1260}{255}$, $\frac{1270}{300}$

KIT DATE 4/13/81
C.R. DATE 4/13/81

ERDMAN, ANTHONY, ASSOCIATES

SHEET 15 OF 15

SUBJECT DAM 564 - CHANNEL SECTION SUB-SHEET NO. 1
PROJECT NAME DAM INSPECTIONS (SU166-00.05)

OWNER

DAM 564 - CHANNEL SECTIONS

SECTION 1 :

$n = 0.095$

$n = 0.05$

$n = 0.045$

40'

7'

20'

I&W = 1293

SECTION 2 & 3 :

$n = 0.075$

$n = 0.05$

$n = 0.075$

50'

7'

20

- I&W = 1287(2), 1262(3)

SECTION 4 :

$n = 0.045$

$n = 0.05$

$n = 0.045$

50

5'

30'

- I&W = 1255

APPENDIX E

INFORMATION AS CONTAINED IN
THE NATIONAL INVENTORY OF DAMS

INVENTORY OF ORANGES

PAGE 125
09/11/1991

